DIFFERENT INDICES FOR VOLTAGE COLLAPSE PREDICTION IN POWER SYSTEM

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Abstract—As the systems power-transmission complexity were increasing in present perspective due to this measurement is becoming complex due to higher order of complexity. Voltage collapse of the system is one of the major fault which leads to the blackouts. If the prediction of this type of fault and any other relative parameters variation by the help of Indices in the system lead to prediction of the variation and preparing for the preventive measures. In this work IEEE 6, 14 and 30 bus system are utilized for the contingency of line outage and several operating conditions. In this work L-Index and its utility is taken in account for numerical calculations and transient process.

I. INTRODUCTION

In present scenario as the power in the pool is becoming more transmission system are operating in security limits. Mostly stability limits are associated to transient and thermal limits of the system. A power system is voltage stable if it maintain the value to voltage to the predisturbance value, similarly it became voltage instable if it is incapable in maintaining pre-disturbance value. As the voltage security of system is V-Q sensitive which helps in determining reactive power demand if less then it system tends to instability and we had to manage the contingency by supply of additional power.

II. VOLTAGE INSTABILITY

In power systems, due to inability of managing system contingency, leads to many unwanted conditions as brownouts, blackouts and security threats. As study of Mechanism for instability of voltage in system, along with instability of voltage Proximity leads to two methods of studying Voltage instability. Load Flow Feasibility (LFF) and Steady State Stability (SSS) are two static methodology.

"Instability of Voltage is majorly a local phenomenon. The objective in research here is to identify faulty location along with instability in voltage identifying the weak bus".

Which are as follows:

- PV curves are utilized in under stressed transmission system findings.
- PV curves are not assigned for weak bus identification.
- PV curve analysis is utility is dependent on application.

III. COLLAPSE OF VOLTAGE IN SYSTEMS

As in power pool; power were regulated by active and reactive flow of power. When system is unable to regulate the desired voltage contingencies occurred in system.

Typical scenario for collapse in voltage are as follows:

- Due to abnormal operation of large machines and their operating parameters few of them are not in contribution.
- As additional reactive power demand create security violation with reduction of voltage along with other operation limits.

1. Voltage stability analysis

There can be various ways to analyze voltage stability, one of them discussed here.

PV and QV curves.

2. PV-QV curve

PV curves: The PV curves are utilized in voltage stability analysis. Theses curves determine Mega Watt distance of the system to voltage collapse center from control center.



Figure 1. Two-bus system

$$P = -\frac{EV}{x}\sin\theta$$
(1)
$$Q = -\frac{V^2}{x} + \frac{EV}{x}\cos\theta$$
(2)

$$= \sqrt{\frac{E^2}{2} - QX \pm \sqrt{\frac{E^2}{4} - X^2 P^2 - XE^2 Q}}$$
(3)

Where P is the total load in an area and V is the voltage of critical bus. A two bus system. Where, active and reactive power respectively are P and Q, consumed by the load, voltage of load bus as V and angle between E and V is θ .

IV. $L_{\mbox{\scriptsize MN}}$ index for stability of line

 L_{mn} represents Index for stability in power line to realize single line diagram, Moghavvemi M. along with Omar [4]. As the proximity of voltage collapse in system lead to security contingencies.



Figure 2. Typical one-line diagram of transmission line.

From power flow equation,

$$S_{i} = \frac{|v_{i}||v_{j}|}{z} \angle \left(\theta - \delta_{i} + \delta_{j}\right) - \frac{|v_{j}|^{2}}{z} \angle \theta$$
(1)

Separating the above equation in real and reactive power then,

V

$$P_{j} = \frac{V_{i}V_{j}}{Z}\cos(\theta - \delta_{i} + \delta_{j}) + \frac{V_{j}^{2}}{Z}\cos\theta$$
(2)

$$Q_j = \frac{v_i v_j}{z} \sin(\theta - \delta_i + \delta_j) + \frac{v_j^2}{z} \sin\theta$$
(3)

Where, $\delta = \delta_i - \delta_j$ and now solving for line voltage as we

$$V_{j} = \frac{V_{i}\sin(\theta-\delta)\pm\{[V_{i}\sin(\theta-\delta)]^{2}-4ZQ_{j}\sin\theta\}^{0.5}}{2\sin\theta}$$
(4)

Substitute
$$Z \sin \theta = X$$

 $[V_{i} \sin \theta]^{2} - 4Q_{j}X \ge 0$ (5) The index of stability for line can be formulated as [4]: $L_{mn} = \frac{4XQ_{j}}{[V_{i} \sin(\theta - \delta)]^{2}} \le 1$ (6)

V. LQP FACTOR OF STABILITY FOR POWER LINE

As given in reference [4] it is defined as:

$$LQP = 4\left(\frac{x}{v_i^2}\right)\left(\frac{xP_i^2}{v_i^2} + Q_j\right)$$

VI. RESULT

For 6 bus system

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(All calculations are on 100 MVA base)
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Table 1 L index at different loading conditions (6 bus system)						
Bus no.	Voltage stability L index					
	Base load	140%	180%	220%	260%	peak load
3	0.1245	0.1821	0.2477	0.3264	0.4299	0.6643
5	0.1031	0.1497	0.2018	0.2618	0.3347	0.4847
6	0.0995	0.1426	0.1922	0.2511	0.3259	0.4809
4	0.0912	0 1 3 3 5	0 1816	0 239	0 3136	0 4761







Table 2 Minimum eigenvalues of reduced Jacobean at different loading conditions (6 bus system)

VII. CONCLUSION

This research work let us know about indexing in the system and comparing the performance of stability. L-Index and traditional counterpart Jacobean for IEEE standard Bus system had to be taken care for contingency analysis of the system. As system parametric variation and its prediction and correction by the algorithms are done, improvised version helps in making system more efficient.

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