A Study on Viscoelastic Surface Instabilities Using Newton Law of Viscosity and Non Newton Law of Viscosity

Dr. Surya Narain Prasad

M.Sc. (Mathematics), Ph.D., SSSUTMS, Sehore

Madhya Pradesh, India.

Abstract

Fluid dynamics is the science which portrays the movement of fluids and their connections with solid bodies. The term fluid is utilized to depict a substance that flows consistently under an applied stress. Much of the time of intrigue, a fluid can be viewed as a continuum, i.e., a nonstop substance. Each point in space has limited qualities for physical properties, for example, velocity, stress, temperature, and so on. Fluids can be delegated Newtonian and non-Newtonian. A Newtonian gooey fluid has a direct connection between the shear stress and the strain rate. A non-Newtonian fluid has a nonlinear wave profile. The consistency of a non-Newtonian fluid shifts with an alternate shear rate in the fluid, the compartment of the fluid, or even the underlying state of the fluid.

Keywords: intrigue, nonlinear, fluid, substance

Introduction

Most of the fluids, for example, artificial fibers, blood, molten plastics, petroleum, ketchup, dyes, and so forth, are considered as non-Newtonian fluids. Such fluids don't comply with the Newtons law of consistency and are typically called as non-Newtonian fluids. The flows of such fluids happen in a wide scope of handy issues having fundamental significance in polymer depolarization, bubble sections, aging, composite preparing, bubbling, plastic froth handling, bubble assimilation and numerous others. In this way, an investigation considering the non-Newtonian conduct of these fluids in such flows appears to be suitable [1]. These fluids can be partitioned into four gatherings: pseudo-plastic, dilatant, Bingham plastic and plastic. A dilatant (shear-thickening) fluid builds obstruction with expanding applied stress. On the other hand, a pseudo-plastic (shear-diminishing), fluid reductions opposition with expanding stress. Bunches of non-Newtonian materials utilized in up to referenced applications show shear-diminishing and shear-thickening attributes which are oftentimes approximated by power-law model [2].

Newtonian Fluids

The hypothesis of fluid mechanics, as portrayed by Sir Isaac Newton, depended on basic shear tests. Specifically, Newton reasoned that the shear stress or power per unit zone F/Aˆ, signified in tensor structure by T, required to deliver movement was relative to the velocity inclination or shear rate ˙γ, indicated as D in tensor structure, and that the steady of proportionality η is the coefficient of shear thickness. This stress constitutive model for Newtonian fluids is summed up scientifically as

$$T=\eta D \qquad (1)$$

The deformation rate tensor D is given by

$$D= \nabla\vartheta + (\nabla\vartheta)^{T} \qquad (2)$$

where the superscript T shows framework interpretation. The consistency η for this situation may not rely upon the shear rates. It is normally basic to characterize the stress tensor and the twisting rate tensor individually as,

$$T=2\eta D, \text{ with } D=1/2\ [\nabla\vartheta + (\nabla\vartheta)^{T}] \qquad (3)$$

A Newtonian fluid is in this way any fluid whose stress constitutive condition for T follows Eq. (3) and whose thickness may fluctuate with fixation, temperature and weight yet may not change with distortion rate, applied stress, time or polymerization rates as on account of responding polymer froths [3]. Run of the mill case of Newtonian fluids incorporate gases, water, low atomic weight inorganic arrangements, liquid metals and salts, straightforward natural fluids, and so forth.

Non-Newtonian Fluids

Non-Newtonian fluid conduct emerges from deviation in both of the two basic attributes of Newtonian conduct. To recap, the two principal normal for Newtonian fluid conduct are (I) a straight stress-strain relationship and (ii) consistency that is autonomous of shear rates, applied stresses, time and response rates [4-6].

Complex fluids, for example, those got from polymers (for example polymer arrangements or dissolves) and micellar arrangements, are worked from a microstructure that comprises of macromolecules. The macromolecular structure fundamentally influences the reaction of the fluid to twisting prompting non-direct conduct between the applied stresses and the subsequent disfigurement rates. The nonlinear stress-strain connections makes these fluids non-Newtonian [7]. The elastic reaction to misshapening because of the macromolecular structure in certainty implies that these fluids display solid like conduct.

Analysis of instability

For all such shear flows, Preziosi and Rionero guarantee to demonstrate security by vitality strategies, yet there is a key mistake in the paper confining its class of bothers to a set which don't fulfill the energy condition; the parent paper by Dunwoody and Joseph, is right yet not pertinent in the constraint of low Reynolds number.

Moving endlessly from Newtonian fluids, the impacts of shear-diminishing have been considered in various calculations by Waters and Keely, khomami [8]. Yield fluids have been concentrated by Pinarbasi and Liakopoulos. Viscoelastic fluids can show a simply elastic flimsiness at their interface, even in the constraint of zero Reynolds number with coordinated viscosities. The direct security of Oldroyd-B and UCM fluids has been researched by Li, and Wilson and Rallison [9].

The elastic instability is driven by a hop in N1 at the interface, and exists in both the long and short wave limits. In the long-wave limit, steadiness relies upon the volume division involved by the more flexible part, however the short-wave limit relies just upon the two materials, and the shear rate at the interface. The instrument of the long-wave flimsiness has been clarified by Hinch et al. Vertical stream, in which the main impetus is gravity instead of an applied weight angle, and will along these lines vary starting with one fluid then onto the next where there is a thickness distinction, has been explored for viscoelastic fluids by Sang.

Larson et al. study visco-elastic hazards in the cutoff that the Re is little. In fact, the favorable position is that the framework is interpretation invariant along the chamber hub (expecting the cell to be exceptionally long) with the goal that one can think about Fourier modes for the spatial balance along the pivot. Since in the $\mathrm{Re} \rightarrow 0$ breaking point inertial impacts are irrelevant, just the distinction in revolution paces of the two chambers matters, so one can for example take the external chamber fixed and study the solidness of the laminar azimuthal stream as an element of the pivot pace of the inward chamber.

For the Oldroyd-B model, Larson et al. [10] anticipated there to be an away from shakiness of the viscoelastic laminar azimuthal base stream: As outlined in Figure. 1a, there is a basic revolution rateΩ_c,

$$\boldsymbol{\Omega_c^2 = \wedge \frac{k_z d}{\Lambda} \frac{d}{R_i}}$$

where $R_i$is the range of the internal chamber, d is the hole between two chambers, kz is the frequency of the velocity adjustment along the chambers, and is a dimensional consistent which is identified with the transient eigenvalue and which relies upon *De*, *kz*, and β. Beyond Ωc, the laminar stream profile is directly precarious to intermittent balances along the pivot of the chamber with the frequency kz showing that past the edge the stream would display a grouped structure extremely suggestive of the Taylor vortices which structure first in the Newtonian situation when passing a basic turn rate. Obviously, the basic worth relies upon the hole to-span proportion of the cell d/Ri, when the range goes to interminability, the unsteadiness vanishes as the edge Ωc movements to vastness. This is predictable with old outcomes that show that viscoelastic planar Couette stream is straightly steady stream all *Wi*.

Utilizing Boger fluids, the primary investigations in [11] effectively affirmed the presence of such an elastic unsteadiness. In more point by point tests a couple of years after the fact, Groisman and Steinberg [12] found that the expectations for the edge revolution rate c additionally concurred quantitatively very well with their exploratory discoveries.

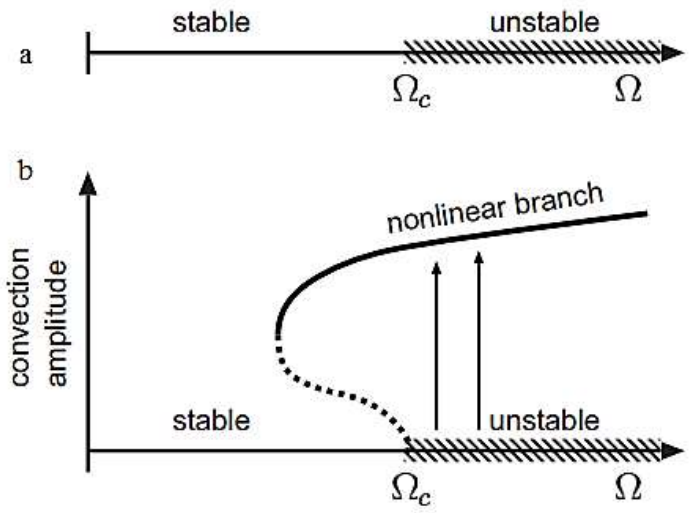

Figure 1a. Sketch of a rotation rate axis, with a critical number a la Larson marked on it. (b) Qualitative sketch of the subcritical scenario as found by Groisman and Steinberg

However, they likewise found that the insecurity is subcritical, as outlined in Figure. 1b once the stream design sets in, limited sufficiency nontrivial stream designs keep on existing when the pivot rate is diminished underneath the basic worth c. In the investigations, the subsequent supposed "di-spin" convection designs are very limited and they keep on existing down to c/2. In this way, these investigations show two significant outcomes: (I) They affirm that with suitably arranged model polymer arrangements, one can reach among tests and hypothetical expectations for Oldroyd-B fluids. (ii) They are the first solid test proof that dangers in quite a while will in general be subcritical, i.e., nonlinearly upgraded.

Linear instabilities general mechanism

It has gotten clear from the work portrayed over that in the little Reynolds number breaking point, visco-elastic flows commonly will in general become directly flimsy because of ordinary stress impacts when the smoothes out are bended. At the point when the Weissenberg number is bigger than around 1, the polymer is extended by the shear angles. The inward piece of the (craftsman impression of) the polymer on the left stretches and pivots, in view of the bigger arch of the smoothes out and the bigger shear close to the inside, towards the circumstance of the subsequent polymer personification on the right. In Figure. 2, we consider a wavy bother along the smoothes out. In the laminar stream condition of the Taylor–Couette calculation, there are bended smoothes out "stacked on head of one another" up and down the hub course. A similar kind of thinking as above prompts the determination that an irritation with a wave vector along the pivot, so the stream moves inwards to some degree at certain levels and moves outwards in areas in the middle of, ought to become temperamental as well. Which unsteadiness is most grounded is a quantitative inquiry which must be settled with an undeniable direct soundness investigation. As Larson et al. discovered, the irritation with wave vector along the pivot ordinarily goes unsteady first, and subsequently the first nontrivial state is a united stream structure, suggestive of Taylor

vortices. There are, be that as it may, locales of boundary space where annoyances with various balance are more flimsy.

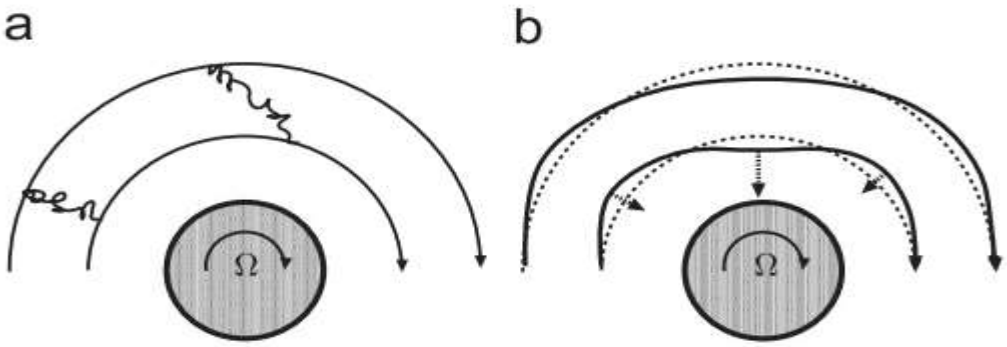

Figure 2. Qualitative sketch of a flow situation with curved streamlines

Pakdel and McKinley [15, 16] have indicated that a large number of the insecurity models dependent on the harmony among shape and ordinary stress impacts can be summed up by a statement of the structure

$$\frac{l}{R}\frac{|N_1|}{\tau_p,shear} > M^2$$

Here *l* is the length scale over which a bother moving along a smooth out will rot; as such, *l= Us1ʎ*, where *Usl* is the normal velocity along the smoothes out and *ʎ*as previously, is the polymer unwinding time. Moreover, R is the regular sweep of shape of the base stream, while in the proportion of the typical stress term N1 and the shear stress τp,shear.

The term $\frac{N_1}{\tau_p}, shear = Wi$is the dimensionless proportion of the anisotropy of the ordinary powers the bigger Wi the bigger this driving term. What's more, the littler the span of bend R, the more grounded the precariousness, thus the term 1/R. At long last, the rot length ought not exclusively be there for dimensional reasons, but on the other hand is considering the physical impact that the more drawn out an irritation endures, the more it can assist with driving the stream flimsy. In this manner, on knowing the past, one could nearly have speculated the overall type of this condition.

At long last, it ought to be stressed that the insecurity condition (11) has not so much been inferred; rather, the status of the condition is more that Pakdel and McKinley saw that all know unsteadiness models could be reworked in this structure, which is physically generally sensible. We are enticed to feel that this condition ought to be seen as a sensible articulation substantial everywhere enough Wiesenberger numbers and not very little radii of ebb and flow. Therefore, the way things are, the above articulation recommends that even at little Wi a flimsiness could set in if the smoothes out are adequately bended. We think of it as more probable, in any case, that such dangers are smothered at little Wi, and that the above articulation ought to be thought of as a decent asymptotic huge Wi dependable guideline which is exact for adequately enormous Wi, bigger than in any event 1. Plainly, this issue should be tended to in more detail later on.

We expect equal visco-elastic shear flows like Poiseuille stream to display a subcritical precariousness to some adjusted or feebly fierce stream state. Visco-elastic mass channel stream would be totally steady, gulf dangers would moist out in adequately long funnels, though if there is a genuine subcritical stream unsteadiness, a bay stream precariousness would trigger sporadic stream in the funnel and henceforth make itself felt all through the extruder. In this sense, the different impacts might be firmly coupled, which makes it hard to make an exact expectation. At the end of the day, if there are, e.g., bay bothers of a given adequacy or inborn mechanical assembly commotion, at that point the subsequent basic Weissenberg number is the one at which the basic sufficiency branch crosses this recommended esteem. In the customary laminar stream system, this unpleasantness is inconceivably little, so it is a straightforward method to portray the anomalies of the surge quantitatively. As demonstrated by the bolts in the figure, when the stream rate is gradually expanded (precious stone images), the soften crack anomalies grow just at a lot higher stream rates than if one gradually diminishes the stream rate (hovers), beginning from the stage where the inconsistencies are available.

Conclusion

Viscoelastic fluids (for instance, polymeric melts and arrangements) have stream properties that are to some extent viscous and to some extent elastic. The nearness of elastic stresses can create hazards, even in idleness less stream, that don't emerge in Newtonian fluids. These are regularly depicted as 'simply elastic' hazards. At the point when polymers are long, they get effectively extended by the shear present in flows, and the viscosity of the arrangement or dissolve is huge. Accordingly, inertial impacts are generally insignificant as the Reynolds numbers are little however the fluid is unequivocally Non Newtonian because of the shear-actuated elasticity and anisotropy, and the moderate unwinding impacts. The dimensionless number overseeing these Non Newtonian impacts is the Weissenberg number Wi. From various exact tests and hypothetical examinations over the most recent fifteen years, it has become evident that as the Weissenberg number increments, visco-elastic fluids show stream insecurities driven by the anisotropy of the typical stress parts and the bend of the smoothes out.

References

Afzal, A. and K. Y. Kim (2013). Mixing performance of passive micromixer with sinusoidal channel walls. *Journal of Chemical Engineering of Japan* 46(3), 230–238.

Alam, A. and K. Y. Kim (2012). Analysis of mixing in a curved microchannel with rectangular grooves. *Chemical Engineering Journal* 181, 708-716.

Cho, C. C., C. L. Chen and C. K. Chen (2012). Mixing of non-Newtonian fluids in wavy serpentine microchannel using electro kinetically driven flow. *Electrophoresis* 33(5), 743–750.

Cook, K. J. and I. Hassan (2013). Experimental and numerical evaluation of a scaled-up micromixer with groove enhanced divisionelements. *Journal of Fluids Engineering* 135(1), 011201–1–14.

Cook, K. J., Y. F. Fan and I. Hassan (2013). Mixing evaluation of a passive scaled-up serpentine micromixer with slanted grooves. *Journal of Fluids Engineering* 135(8), 081102–1–12.

Du, Y., Z. Zhang, C. Yim, M. Lin and X. Cao (2010). Evaluation of floor-grooved micromixers using concentration-channel length profiles. *Micromachines*1, 19–33.

Fellouah, H., C. Castelain, A. Ould-El-Moctar and H. Peerhossaini (2010). The Dean instability in power-law and Bingham fluids in a curved rectangular duct. *Journal of Non-Newtonian Fluid Mechanics* 165(3-4), 163–173.

Liu, S., A. N. Harymak and P. E. Wood (2006). Laminar mixing of shear thinning fluids in a SMX static mixer. *Chemical Engineering Science* 61(6), 1753–1759.

Rahmani, R. K., T. G. Keith and A. Ayasoufi (2004, July). Numerical simulation and mixing study of non-Newtonian fluids in an industrial helical static mixer. In *Proceedings of the ASME Heat Transfer/Fluids Engineering Summer Conference*, New York, USA.

Scherr, T., C. Quitadamo, P. Tesvich, D. S. W. Park, T. Tiersch, D. Hayes, J. W. Choi, K. Nandakumar and W. T. Monroe (2012). A planar microfluidic mixer based on logarithmic spirals. *Journal of Micromechanics and Microengineering*22(5), 055019–1–10.

Tsai, R. T. and C. Y. Wu (2011). An efficient micromixer based on multi directional vortices due to baffles and channel curvature. *Biomicrofluidics*5(1), 014103–1–13.

Vanka, S. P., G. Luo and C. M. Winkler (2004). Numerical study of scalar mixing in curved channels at low Reynolds numbers. *American Institute of Chemical Engineers Journal* 50(10), 2359–2368.

Wang, H., P. Iovenitti, E. Harvey and S. Masood (2003). Numerical investigation of mixing in micro channels with patterned grooves. *Journal of Micromechanics and Micro engineering* 13(6), 801–808.