

# Space Vector Modulation Based Three-Phase PWM Rectifier Voltage Oriented Control

Dr. S. Siva Prasad<sup>1</sup> Ch.Vikram<sup>2</sup>

<sup>1</sup>Professor, <sup>2</sup>Assistant Professor,

<sup>1,2</sup>Department of EEE, Vidya Jyoti Institute of Technology, Hyderabad, Telangana state.

**Abstract:** The flow challenges urge the analysts to structure and advance the devices allowing the transformation and the control of energy. The power converters comprise in adjusting the wellspring of vitality to the requirements for the heap. In this paper, we present the investigation of voltage oriented control space vector modulation (VOC-SVM) methodologies for three-stage PWM rectifiers. This system of control established on the change between stationary directions  $\alpha$ - $\beta$  and synchronous rotating facilitates d-q, it depends on the input– output criticism linearization controller for which the goal is to control the framework current's d-and q-load part, while the dc-transport voltage is kept up at the ideal dimension and fulfil the solidarity control factor (UPF) activity. The system VOC-SVM guarantees high static execution and quick transient reaction by utilizing inward current control circle. In addition, the examinations were done by utilizing simulation under nature Matlab/Simulink.

**Index terms:** Voltage arranged control; PWM rectifier; Space vector balance; Input– output criticism linearization.

## I. INTRODUCTION

A few mountings of three-stage PWM rectifiers are utilized in various mechanical divisions require critical power. In fact, these converters are nonlinear burdens which ingest non-sinusoidal flows and expend the responsive power which prompts a low power factor and a mutilation of the line voltage [1]. Thus, the three- stage PWM rectifiers are a standout amongst the most encouraging arrangements because of favourable circumstances, for example, the utilization of a present near a sinusoid by diminishing its consonant substance, the receptive power control assimilated and the dc-transport voltage and guaranteed it a bidirectional exchange of intensity [2]. The control of the PWM rectifier can be viewed as a typical issue with controlling a PWM inverter. A few methods of control of PWM converters were displayed in the writing which intends to have a diminished symphonies mutilation proportion and an exact power control [3-4]. They can be ordered, as indicated by their standards in two classes: procedures dependent on the voltage and strategies based on the virtual-transition which were planned in [5] - [9]. The DPC techniques intends to wipe out the beat width adjustment square and the inside control circle by supplanting them with an exchanging table whose inputs are the mistakes between the reference esteems and the deliberate qualities and were created in [6-7],[10],[12]. The VOC technique is established on the facilitates change between the fixed directions framework  $\alpha$ - $\beta$  and arranges d-q, where the present control is conveyed in the voltage space vector of reference outline situated [2-3], [14]. In this paper, we propose another way to deal with control the three-stage PWM rectifiers which is the VOC with space vector tweak (SVM). For this we have executed a non-straight control strategy that considers non-linearity of the framework, this technique depends on an information yield input linearization so it guarantees, the control of the dc-transport voltage and the flows ( $i_d$ - $i_q$ ) and furthermore guarantee solidarity controlfactor.

## II. MATHEMATICAL MODEL

Fig. 1 demonstrates the square graph of the three-stage PWM rectifier, in which  $e_a$ ,  $e_b$  and  $e_c$  speak to the power source stage voltages;  $R$  and  $L$  is line obstruction and line inductance individually;  $i_a$ ,  $i_b$  and  $i_c$  are the line current of PWM rectifier;  $v_a$ ,  $v_b$  and  $v_c$  are the AC side voltages of the rectifier;  $C$  is dc-connect capacitor;  $i_{dc}$  is dc-interface current;  $i_L$  is load current;  $R_L$  is load opposition. From Fig. 1, we can deduct the conditions of the framework in the two-stage synchronous revolution d-q-organize:

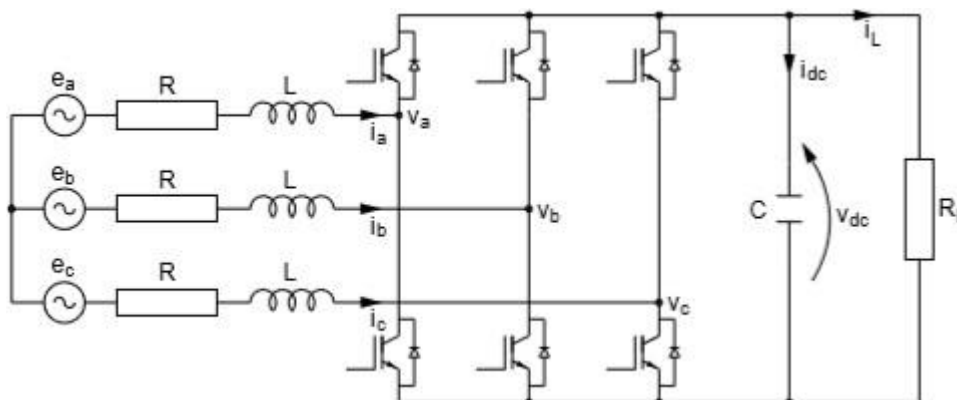


Fig 1.Schematic diagram of a PWM rectifier

$$\left. \begin{aligned} \frac{di_d}{dt} &= \frac{-R}{L} i_d + \omega i_q + \frac{1}{L} (e_d - v_d) \\ \frac{di_q}{dt} &= \frac{-R}{L} i_q - \omega i_d + \frac{1}{L} (e_q - v_q) \\ \frac{dv_{dc}}{dt} &= \frac{-v_{dc}}{L} + \frac{(e_d i_d + e_q i_q)}{C V_{dc}} \end{aligned} \right\} \quad (1)$$

**III. PRINCIPLE OF VOLTAGE ORIENTED CONTROLSPACE VECTOR MODULATION**

*System configuration*

VOC depends on the introduction of the present vector a similar way as that of the voltage vector, by controlling the present vector in the two pivoting facilitates dq. This control technique it conceivable to deal with the two parts of the present vector in the synchronous directions coordinated a similar way of the voltage vector of the framework. This which guarantees the PWM rectifier should draw of the sinusoidal line flows. This structure present a noteworthy hindrance lies in its variable exchanging recurrence. A motivation behind acquiring a steady exchanging recurrence, one uses the VOC-SVM. Therefore, the exhibitions of the control firmly rely upon the capacity of the control circle input-yield criticism linearization controller [8],[11], [14]. As appeared in Fig.2, the all out topology of the voltage situated control with space vector balance for a three-stage PWM rectifier, Sa, Sb and Sc speak to the exchanging condition of the rectifier; id-q are d-q parts of the matrix current; ed-q are d-q segments of the framework voltage; ud-q are d-q segments of the information voltage of the rectifier; uα-β are α-β segments of the information voltage of the PWM rectifier. The VOC depends on the synchronization by the PLL (Phase Locked Loop) to gauge and channel the edge of the source and the momentary adequacy of the identical period of a three-stage framework. The PLL ensure that it pursued by period of the immediate segment of the network voltage, ed, so as to take out the part in squaring, eq, which delivers the evaluated stage, θ, is equivalent to the period of the matrix[9].

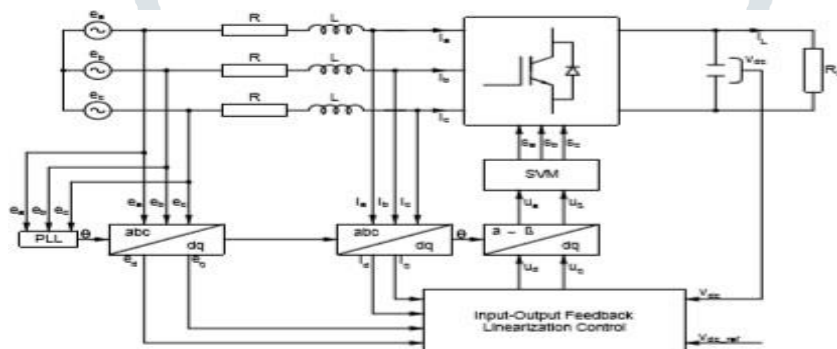


Fig. 2. Configuration of VOC for PWM rectifier

For the change of directions  $\alpha$ - $\beta$  to the coordinates d-q the point of voltage vector is given by:

$$\sin\theta = \frac{e_\beta}{\sqrt{(e_\alpha)^2 + (e_\beta)^2}} \quad (2)$$

$$\cos\theta = \frac{e_\alpha}{\sqrt{(e_\alpha)^2 + (e_\beta)^2}} \quad (3)$$

#### IV. SVPWM GENERATION

The Pulse Width modulation technique permits to obtain three phase system voltages, which can be applied to the controlled output. Space Vector Modulation (SVM) principle differs from other PWM processes in the fact that all three drive signals for the inverter will be created simultaneously. The implementation of SVM process in digital systems necessitates less operation time and also less program memory.

The SVM algorithm is based on the principle of the space vector  $u^*$ , which describes all three output voltages  $u_a$ ,  $u_b$  and  $u_c$ .

$$u^* = \frac{2}{3} \cdot (u_a + a \cdot u_b + a^2 \cdot u_c) \quad (4)$$

Where  $a = -1/2 + j \cdot \sqrt{3}/2$

We can distinguish six sectors limited by eight discrete vectors  $u_0 \dots u_7$  (fig: - inverter output voltage space vector), which correspond to the  $2^3 = 8$  possible switching states of the power switches of the inverter.

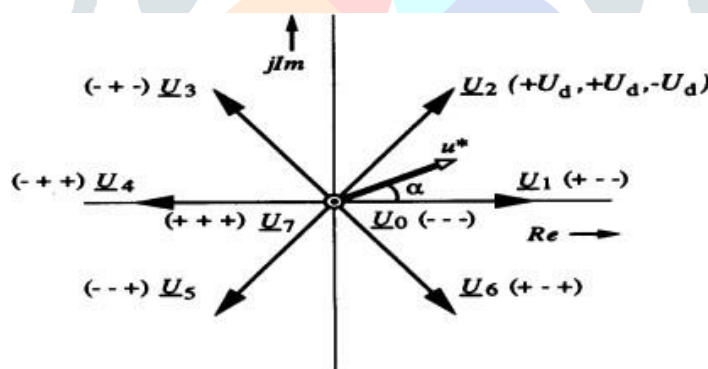


Fig. 3. Space vector Modulation

The amplitude of  $u_0$  and  $u_7$  equals 0. The other vectors  $u_1 \dots u_6$  have the same amplitude and are 60 degrees shifted.

By varying the relative on-switching time  $T_c$  of the different vectors, the space vector  $u^*$  and also the output voltages  $u_a$ ,  $u_b$  and  $u_c$  can be varied and is defined as:

$$u_a = \text{Re}(u^*) \quad (5)$$

$$u_b = \text{Re} ( u^* \cdot a-1) \tag{6}$$

$$u_c = \text{Re} ( u^* \cdot a-2) \tag{7}$$

During a switching period  $T_c$  and considering for example the first sector, the vectors  $u_0$ ,  $u_1$  and  $u_2$  will be switched on alternatively.

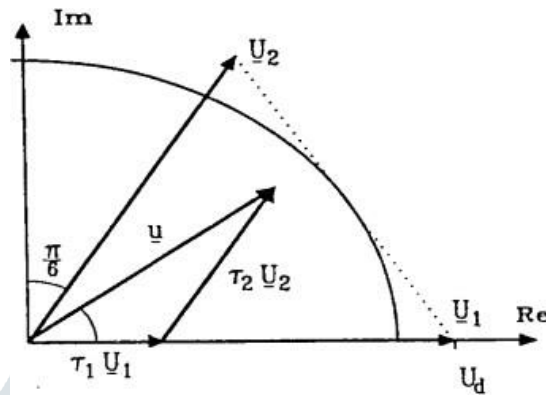


Fig. 4. Definition of the Space vector

**V. PRINCIPLE OF THE INPUT OUTPUT FEEDBACK LINEARIZATION CONTROLLER**

The information yield criticism linearization control approach permits of numerically changing the non-direct framework in a halfway or totally straight framework so as to have utilized the direct control strategies.

Either the framework characterized by:

$$\dot{x} = f(x) + g(x)u \tag{8}$$

$$y = h(x) \tag{9}$$

Or

$x = [x_1, \dots, x_n]^T$  is the vector of the states,

$u = [u_1, \dots, u_p]^T$  is the vector of the controls,

$y = [y_1, \dots, y_r]^T$  represents the vector of the output,  $f(x)$ ,  $g(x)$  and  $h(x)$  are non-linear functions.

This control technique consists in finding a relation linear between the input and the output by deriving the output until at least an entry appears by using the expression:

This control system comprises in finding a connection straight between the info and the yield by determining the yield until somewhere around a section shows up by utilizing the articulation:

$$y^{(r_j)} = L_f^{(r_j)} h_j(x) + \sum_{i=1}^p L_{g_i}(L_f^{(r_j-1)} h_j(x)) u_i \tag{10}$$

Or:

$$L_{g_i} L_f^{(r_j-1)} h_j(x) \neq 0 \tag{11}$$

$r_i$  is the relative degree of the system.

The derivatives of Lie are defined by the following relationship:

$$L_f h(x) = \left( \frac{\partial h(x)}{\partial x} \right) \quad \text{---} \quad (12)$$

By iteration (12), we have the following equation:

$$L_f^i h_j = (L_f^{i-1} h_j); i = 2, 3, \dots \quad (13)$$

The expression (13) can be written in following matrix form:

$$\begin{bmatrix} y_1^{r1} \\ \vdots \\ y_p^{rp} \end{bmatrix} = \begin{bmatrix} L_f^{r1} h(x) \\ \vdots \\ L_f^{rp} h_p(x) \end{bmatrix} + D(x)u \quad (14)$$

Or  $D(x)$  is the matrix of decoupling of the system.

The control law for linearization and decoupling input-output is given by:

$$[u] = D(x)^{-1}[-A(x) + [V]] \quad (15)$$

Or:

$[v] = [v_1 \ v_2 \ \dots \ v_p]^T$  represents the new vector of the input variables.

Substituting (15) in (14), the equivalent system becomes linear and totally decoupled from the form:

$$\dot{y}_p = [V_1, \dots, V_p]$$

The variables  $v_i$  and  $y_i$  can be determined from dynamic equations of the errors.

## VI. CONCLUSION

This work proposes the displaying and re-enhancement of voltage arranged control space vector tweak dependent on nonlinear control of PWM rectifier. The scientific models of the worldwide framework are introduced. The recreation results demonstrated this proposed procedure and demonstrated their viability into keep up the dc-transport voltage and the current at the ideal dimension, just as music decrease. The proposed system gives great static, unique exhibitions by means of inside current control circle and has a fantastic vigour.

## REFERENCES

- [1] KE-XIN, W., & SHUI-MING, W. (2008, December). Displaying and recreation of three-stage voltage source PWM rectifier. In *Advanced Computer Theory and Engineering, 2008. ICACTE'08. Global Conference on* (pp. 982-986). IEEE.
- [2] MALINOWSKI, M., KAZMIERKOWSKI, M. P., & TRZYNADLOWSKI, A. (2003). Audit and relative investigation of control systems for three-stage PWM rectifiers. *Mathematics and Computers in Simulation*, 63(3), 349-361.
- [3] KAZMIERKOWSKI, M. P. (2002). Direct power control of three-phase PWM rectifier utilizing space vector modulation simulation examines. In *Industrial Electronics, 2002. ISIE 2002. Procedures of the 2002 IEEE International Symposium on* (Vol. 4, pp. 1114-1118). IEEE.
- [4] BOUAFIA, A., GAUBERT, J. P., & KRIM, F. (2010). Prescient direct power control of three-stage beat width adjustment (PWM) rectifier utilizing space-vector balance (SVM). *Power Electronics, IEEE Transactions on*, 25(1), 228-236.
- [5] MALINOWSKI, M., KAZMIERKOWSKI, M. P., AND TRZYNADLOWSKI, A. M. (2003). A near investigation of control procedures for PWM rectifiers in AC movable speed drives. *Power Electronics, IEEE Transactions on*, 18(6), 1390-1396.
- [6] NOGUCHI, T., TOMIKI, H., KONDO, S., AND TAKAHASHI, I. (1998). Direct power control of PWM converter without power source voltage sensors. *Industry Applications, IEEE Transactions on*, 34(3), 473-479.
- [7] LOURCI, N., LALLI, D., MELLIT, A., MEDIATED, B., & BERKOUK, E. M. (2011). Control of input output feedback linearization and varying step size Maximum power point tracking algorithm for a grid-connected photovoltaic inverter. *Renewable energy*, 36(12), 3282-3291.
- [8] GAYNOR, P., & ACHARYA, P. (2013). Direct Power Control Space Vector Modulation Approach Suitable for Turbines running at Changeable Speeds.
- [9] YIN, H., & DIECKERHOFF, S. "Experimental comparison of DPC and Voltage Oriented Control of a three-level NPC grid coupled converter". In *Power Electronics for Distributed Generation Systems (PEDG), 2015 IEEE 6th International Symposium on* (pp. 1-7). IEEE, 2015.
- [10] OTTERSTEN ROLF. "On Control of Back-to-Back converters and Sensorless Induction Machine Drives". PhD Thesis, Department of Electric Power Engineering, Chalmers University of Technology, Göteborg, Sweden, 2003. 165p. ISBN :91-7291-296-0.
- [11] RODRIGUEZ J.R., DIXON J.W., ESPINOZA J.R., PONTT J., LEZANA, P. "PWM Regenerative Rectifiers: State of the Art". *IEEE Transactions on Industrial Electronics*, 2005. Vol.52, issue: 1. Pages: 5-22.
- [12] RUNXIN WANG, JINJUN LIU. "Redefining a New-Formed Average Model for Three-Phase Boost Rectifiers/Voltage Source Inverters". *Applied Power Electronics Conference and Exposition, 2009*. Pages: 1680-1686.
- [13] WANG XU, HUANG KAIZHENG, YAN SHIJIE, XU BIN. "Simulation of Three-phase Voltage Source PWM rectifier Based on Space Vector Modulation". *Control and Decision Conference, Chinese, IEEE 2008*. Pages: 1881-1884.
- [14] WEI KE-XIN, WANG SHUI-MING. "Modeling and Simulation of Three-Phase Voltage Source PWM Rectifier". *International Conference on Advanced Computer Theory and Engineering, IEEE 2008*, Pages: 982-986.