

SOLID DYNAMICS USING NON-LINEAR MATHEMATICAL SIGMUND MODEL AND SLOPE FUNCTIONS

R.Geetha
Asst.professor
Dept of mathematics
AJK College of Arts and Science

Abstract

The type of a nonlinear shift in weather conditions condition with a fourth request diffusive term. This halfway differential condition concedes stun wave arrangements with a chosen velocity, which compare to soak engendering ventures at first glance. This choice mechanism gives an exact trial of the vehicle and sputtering forms at first glance. Our condition likewise gives a productive methods for mimicking sputtering impacts on any surface with locales of high slope. This paper portrayed to Non-Linear mathematical Sigmund model slope capacities are handled into solid dynamics.

Keywords: Solid Dynamics, Mathematical, Slope, Non-Linear, Sigmund Model.

1. Introduction

In functional building applications including to a great degree complex geometries, fitting normally speaks to an expansive segment of the general plan and examination time. In the computational mechanics network, the capacity to perform figurings on tetrahedral networks has turned out to be progressively imperative. Therefore, the robotized tetrahedral work generators by methods for Delaunay and propelling front procedures have as of late gotten expanding consideration in various imperative application zones, for example, cardiovascular tissue modeling, crash affect reenactment, impact and break mechanics and complex multi-material science issues. Tragically, current tetrahedral component innovation in solid mechanics (e.g. ANSYS AUTODYN, LS-DYNA, ABAQUS/Explicit, Altair HyperCrash), ordinarily dependent on the utilization of the customary Finite Element based second request removal plan, has a few unmistakable weaknesses, in particular: (1) Reduced request of union for strains and stresses; (2) High recurrence clamor in the region of stuns; (3) Stability issues related to shear locking, volumetric bolting and weight checkerboard dangers.

To address the deficiencies specified over, a wide assortment of upgraded discretisation advances have been produced. For instance, for the instance of almost incompressible materials, the mean dilatational hexahedral detailing where steady introduction is utilized for the count of volumetric burdens has pulled in modern enthusiasm, as the alterations related to the traditional dislodging based plan are minor. High request components (otherwise called p-refinement) can on the other hand be utilized. Be that as it may, the expansion in the quantity of reconciliation focuses can definitely diminish the computational productivity of these plans in correlation with low request approaches, uncommonly when either complex constitutive laws

(i.e. anisotropic visco-versatile models are frequently utilized in the therapeutic field or contact surfaces, or a mix of both, must be modeled.

All the more as of late, the p-F detailing was enhanced on account of about incompressible materials, by methods for an extra protection law for the Jacobian of the twisting J (broadly known as volume delineate law, giving additional adaptability to the figuring of the volumetric pressure. This inventive thought broadened the scope of utilization of the plan to about and completely incompressible media. In addition, further improvement of the structure has as of late been accounted for by the creators, while considering materials represented by a poly raised constitutive law, empowering the symmetrisation of the subsequent hyperbolic system of equations.

2. Sigmund Model

As indicated by Sigmund, the probability of a particle being removed from the objective surface is essentially relative to the aggregate vitality that achieves the molecule from close-by particle impact forms. The key disentanglement is to assume that every particle enters a separation a beneath the surface as estimated along its direction, whereupon the particle vitality is discharged in a Gaussian dissemination with widths σ along the direction and μ opposite to it. This straightforward picture depends on Sigmund's prior work on answers for the Boltzmann transport equation and is the beginning stage for a significant part of the hypothetical work in sputtering.

In cartesian coordinates, the surface is conveniently described by a height function $z = h(x, y)$, with the ion trajectories along the z-axis. The distribution of energy due to an ion at (x', y', z') is

$$E(x, y, z; x', y', z') = \frac{\epsilon}{(2\pi)^{3/2}\sigma\mu^2} \exp\left(-\frac{(z' - z)^2}{2\sigma^2} - \frac{(x' - x)^2 + (y' - y)^2}{2\mu^2}\right)$$

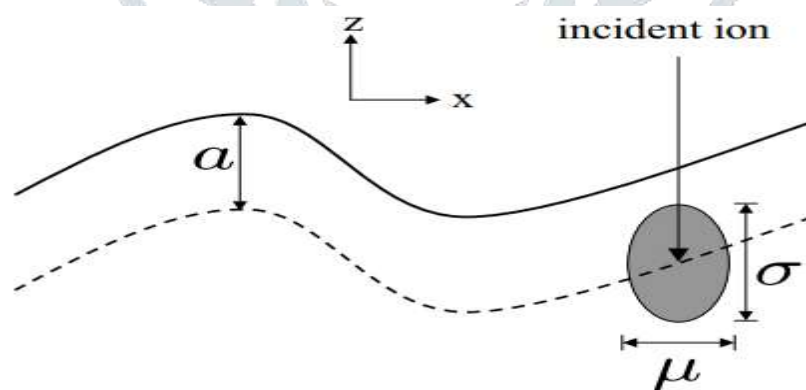


Figure 1: Schematic picture of Sigmund model

2.1 The One Dimensional Description

The one dimensional depiction When the span of a pit is expansive contrasted with the length parameters in the Sigmund model (a, σ, μ), just like the case for the investigations we are examining, it does the trick to regard the edge as being straight and to think about its profile as a one dimensional advance.

Consequently we will work in the farthest point that the surface geometry is translationally invariant in the y heading, except if expressed something else.

$$\frac{h}{\sqrt{1+h'(x)^2}} = -\frac{1}{2\pi T_s} \int dx' \exp \left[-\frac{(h(x') - a - h(x))^2}{2\sigma^2} - \frac{(x' - x)^2}{2\mu^2} \right]$$

where \dot{h} and h' denote differentiation in time and space, respectively. We introduce the time constant

$$T_s \equiv \frac{\sigma\mu}{pJ\epsilon}$$

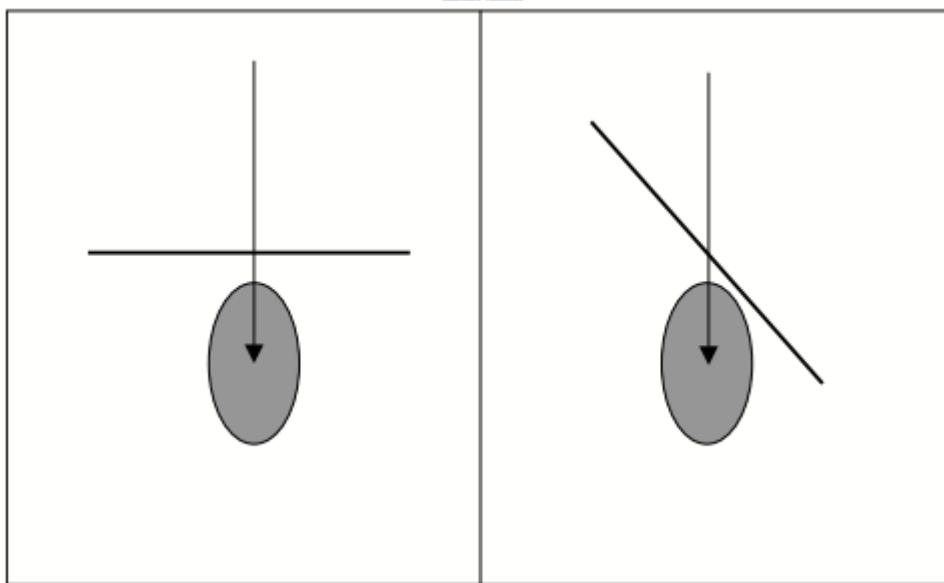


Figure 2: The ion is closer to the surface when the slope is nonzero (right) compared to the zero slope case (left). However, the flux per surface area is reduced on the right

2.2 Planar Unit

To gain intuition the simplest case of a flat surface,

$$h(x) = bx + h_0$$

with b constant. The integral Gaussian and evaluates to

$$\frac{\sqrt{2\pi}\mu}{\sqrt{1+b^2\frac{\mu^2}{\sigma^2}}} \exp \left[-\frac{a^2/\sigma^2}{2(1+b^2\frac{\mu^2}{\sigma^2})} \right] \equiv I(b)$$

This expression has a simple interpretation. In the exponent, the slope b effectively reduces the penetration depth, because for off-normal incidence, the ion stops closer to the surface.

3. A local approximation to the Sigmund model

With the end goal to think about the dynamics of surfaces, we have to portray surfaces that are not level. Since we have seen that the Sigmund vital is Gaussian for a steady slope, we are prompt think about a surface with gradually fluctuating slope, one might say to be made exact right away. This will yield a nearby depiction of the Sigmund model as an incomplete differential equation (PDE). The striking component of this PDE is that it portrays surfaces of discretionarily huge slopes, as on account of the pit edge. We should figure the surface velocity at $x = 0$, with the end goal that the surface has the extension

$$h(x) = h_0 + bx + \frac{\eta}{2}x^2 + \dots$$

what's more, has slope b at the starting point and second subsidiary η . We wish to discover the adjustment to the level surface advancement to driving request in η . Dropping the prime in the fake variable, the fundamental progresses toward becoming

$$\int dx \exp \left[-\frac{(bx - a + \eta x^2/2)^2}{2\sigma^2} - \frac{x^2}{2\mu^2} \right]$$

which to first order in η is

$$\int dx \exp \left[-\frac{(bx - a)^2}{2\sigma^2} - \frac{x^2}{2\mu^2} \right] \left(1 - \frac{\eta x^2}{2\sigma^2} (bx - a) \right)$$

This vital comprises of a Gaussian duplicated by another capacity. On the off chance that this capacity shifts gradually over the width of the Gaussian, at that point our guess is great, and we can disregard higher subsidiary terms in the Taylor development of $h(x)$. In the wake of finishing the square in the example, the width Δ of the Gaussian is observed to be

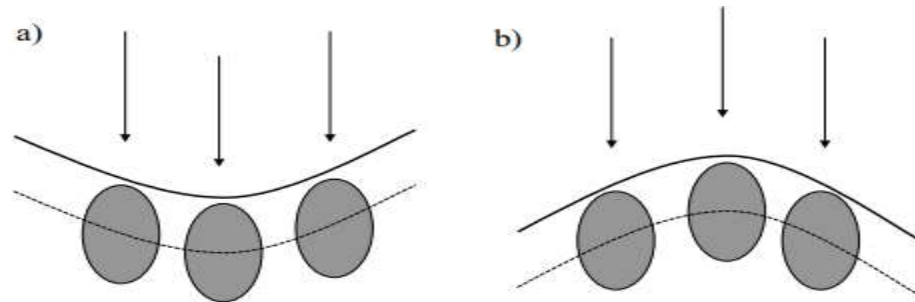
$$\frac{1}{\Delta^2} = \frac{b^2}{2\sigma^2} + \frac{1}{2\mu^2}$$

The η -independent term is while the order η integral evaluates to

$$a\mu\sqrt{\frac{\pi}{2}} \left(\frac{\mu^2}{\sigma^2} \right) \frac{-2b^4\mu^4/\sigma^4 + (a^2/\sigma^2 - 1)b^2\mu^2/\sigma^2 + 1}{(1 + b^2\mu^2/\sigma^2)^{7/2}} \exp \left[-\frac{a^2/\sigma^2}{2(1 + b^2\mu^2/\sigma^2)} \right] \eta$$

Despite the fact that we have picked ordinary rate, our formalism really contains all frequency points on the grounds that any rate edge can be conveyed to zero by appropriately tilting the surface, that is, moving

the slope by a consistent. "Frequency edge" and "point of surface tendency" are identical. Thus the majority of our outcomes will hold for any rate edge through a revolution or projection. Different creators have worked in a nearby organize system wherein the slope is locally zero by moving the frequency edge. This unnecessarily confuses matters, and powers one to take the little slope restrain with the end goal to interface



locales of various slopes.

Figure 3: Sigmund sputtering of a valley (a) and a crest (b)

It ought to be noticed that the story is more muddled for genuine surfaces in light of the fact that, notwithstanding swells, the hazards can be characteristically two dimensional. An emotional case of such a shakiness which we call "grass" or "hair". Obviously this can't be portrayed with a one dimensional model. Beside two dimensional insecurities, swell instabilities are additionally trickier in light of the fact that rotational symmetry is broken. The swells must pick an introduction. At ordinary rate, this should be possible by, say, the raster design. For off ordinary frequency, swells regularly either shape parallel to the particle direction (as observed from above) or opposite to it. For exceptionally diagonal frequency, the previous is the situation. For near ordinary frequency, we have the last mentioned, which can be examined in our one dimensional depiction. At moderate occurrence points, the two introductions contend, and the slope at with D (b) ends up positive denotes the edge past which swells will dependably be parallel.

3.1 Slope Evolution

This condition holds for the pit tests we are thinking about. Since the rate of sputtering is unaffected by a uniform move in surface tallness, it is advantageous to consider rather the advancement of the slope. Separating on the two sides, we find

$$\frac{\partial b(x,t)}{\partial t} = - C(b(x,t)) \frac{\partial b(x,t)}{\partial x} + \frac{\partial}{\partial x} \left(D(b(x,t)) \frac{\partial b(x,t)}{\partial x} \right) - B \frac{\partial^2}{\partial x^2} \frac{1}{\sqrt{1+b^2}} \frac{\partial}{\partial x} \frac{b_x}{(1+b^2)^{3/2}}.$$

In the above we have defined the nonlinear velocity

$$C(b) \equiv \frac{\partial}{\partial b} F(b),$$

A nonlinear shift in weather conditions dispersion equation for the slope, with velocity $C(b)$ and diffusivity $D(b)$ the two elements of the slope, with an extra surface dissemination term. We take this PDE to be our nonlinear model of surface dynamics under particle sputtering.

3.1.1 Slope versus curvature

Review that our shift in weather conditions dissemination PDE originates from a systematic extension of the Sigmund vital. To decide the viability of this development, we kill the second request (hostile to)diffusive term (while holding surface dissemination). We see that the shift in weather conditions alone is a sensible portrayal of sputtering. This isn't astounding given that the profile is at a length scale a lot bigger than the sputtering parameters. Inconsistencies show up at the best and base of the main edge, where bend is generally obvious.

3.1.2 Step velocity

We'd like to predict the velocity of the leading edge as a function of the parameters. Clearly this is given by the difference between the sputtering rate of the edge region and the horizontal rate, divided by the edge slope:

$$U = \frac{F(b) - F(0)}{b}$$

where b alludes to the slope of the lofty driving edge. Note this is the Rankine Hugoniot condition commonplace from stun hypothesis, which we address in the following segment. This connection between the velocity and the slope of the edge locale, and where along this bend are our recreations. The shift in weather conditions velocity $C(b)$ will in general zero for diminishing slope, with the goal that a mound profile in the slope, relating to a stage at first glance, will be "settled" at the base amid shift in weather conditions. As the protuberance voyages, the base part will haul behind, and since the zone under the mound (equivalent to the progression tallness) is monitored, its adequacy must reduce in time. This is known as rarefaction and has the impact of spreading out the surface advance, with the goal that a propelling pit edge will in the end turn out to be less steep. There is a window of time in which the upper bit of the progression stays soak. In real analyses, the pits stay soak for the term of the investigation; this is conceivably because of upgraded disintegration at the base of the progression from reflected particles.

Conclusion

Both the stun velocity and the drawing rate of a level surface scale as μ/T_s , their proportion is a dimensionless number that depends just on the state of the sputter yield versus slope, i.e., the dimensionless parameters a/σ , μ/σ , and Σ . This is an extreme trial of the hypothesis in light of the fact that these parameters

can be removed by fitting. It depends certainly on the sputter parameters which administer the yield as an element of slope. Note that the surface dissemination consistent B does not show up in light of the fact that it just influences the sharpness of the stun wave, not its velocity.

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