

BUCKLING ANALYSIS OF DIESEL ENGINE CONNECTING ROD FOR DIFFERENT LOAD CONDITIONS

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ABSTRACT

The interfacing bar is the momentary part between the cylinder and the driving rod. Its fundamental limit is to send the push and pull from the cylinder pin to the wrench pin, thusly changing over the responding movement of the chamber into turning development of the wrench. The limit of associating pole is to communicate the push of the cylinder to the driving rod, and as the result the responding movement of the cylinder is deciphered into rotational development of the wrench shaft. It contains a pin-end, a shank area and a wrench end. Pin end and wrench end pin gaps are machined to permit definite fitting of heading. One finish of the interfacing pole is related with the chamber by the chamber pin. Interfacing poles are exposed to powers created by mass and fuel ignition. These two qualities bring about hub burden and bowing anxieties. A partner bar must be prepared for sending hub pressure, pivotal pressure, and bowing pressure achieved by the push and pull of the chamber and by radial power. In this postulation, an associating bar is shown using catiav5, discretization using Hyper Mesh and investigation using Nastran. The result predicts the most outrageous clasping burden and

essential area on the interfacing shaft. It is basic to locate the fundamental domain of concentrated worry for fitting changes. To find the burdens made in interfacing post under static stacking with different stacking conditions of pressure and strain at wrench end and pin end of associating bar.

1. INTRODUCTION

In this paper, one fragment of an engine explicitly, the interfacing pole, will be penniless down. Being a victor among the most crucial parts in a motor's outline, the interfacing shaft must be able to withstand huge loads and communicate an impressive proportion of power. It is nothing unexpected that a disappointment in a partner bar can be one of the costliest and harming dissatisfactions in a motor. Notwithstanding, essentially saying that isn't sufficient to absolutely understand the components of the circumstance.

The interfacing bar is the temporary part between the chamber and the crankshaft. Its key breaking point is to transmit the push and draw from the chamber pin to the wrench pin, thusly changing over the reacting development of the

chamber into turning improvement of the wrench. The restriction of partner bar is to communicate the push of the chamber to the wrench shaft, and as the outcome the reacting development of the chamber is interpreted into rotational improvement of the wrench shaft. It incorporates a pin0end, a0shank fragment and a wrench end. Pin0end and wrench end0pin holes are machined to0permit accurate0fitting obviously. One finish of the interfacing bar is associated with the chamber by the barrel pin. Interfacing bars are exposed to qualities delivered by mass and fuel start. These two characteristics bring about urgent burden and bowing weights. An accomplice bar must be ready for communicating urgent weight, center point weight, and bowing tension accomplished by the push and draw of the chamber and by outspread force..

2. LITERATURE REVIEW

Associating bar in an inward burning motor is exposed to joined gas power and idleness powers because of mass which brings about pivotal and bowing anxieties. Bowing anxieties are because of whimsies, driving rod, Case divider disfigurement and rotational mass power. In this way an interfacing bar must be equipped for communicating pivotal pressure, hub pressure and bowing burdens brought about by cycle on the cylinder and by diffusive power. In this work the interfacing bar of a Kirloskar TV1 diesel motor creating an evaluated yield of 5.2Kw at 1500rpm is considered for the investigation. Burden bends are gotten from the weight – wrench point plots. Gas powers and dormancy powers are determined from these bends. Limited component investigation programming ANSYS is utilized to examine the pressure circulation and disfigurement in the

interfacing bar. The measurements are truly estimated to acquire the CAD model of interfacing bar in CATIA V5. Since the heaviness of the interfacing bar has significant impact on its dynamic conduct, an advancement study was performed on a steel produced associating pole with a thought for decrease in weight.

The interfacing pole is the middle of the road part between the cylinder and the Crankshaft. Its essential capacity is to send the push and pull from the cylinder pin to the wrench pin, consequently changing over the responding movement of the cylinder into turning movement of the wrench. This report depicts planning and Analysis of associating pole just as finding

substitute material for associating bar. Presently existing associating pole is made by utilizing Carbon steel. In this drawing is drafted from the figurings. A parametric model of Connecting bar is displayed utilizing CATIA V5 R21 programming and to that model, examination is done by utilizing ANSYS 18.1 Software. Limited component investigation of interfacing pole is finished by thinking about the materials, viz. SAE 4340, 42CrMo4 and Al 7075-T651. The best blend of boundaries like Von misses Stress and strain, Deformation, Factor of security and weight decrease for uncompromising vehicle cylinder were done in ANSYS programming. The current work has been set up to supplant the current interfacing pole made of produced steel with the aluminum MMC associating bar for weight advancement..

3. FINITE ELEMENT ANALYSIS

. The underneath figure shows the mathematical model of an associating bar utilized in a two-

chamber SI Engine. The displaying has been finished utilizing the demonstrating programming, CATIA v5. It contains a cylinder end, shank and a wrench end partitioned into two sections for simpler establishment. For model disentanglement, all filets and chamfers underneath 3mm are ignored and the last model is spoken to in the above figure.

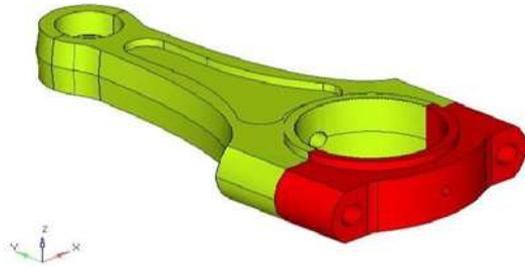


Figure Geometric model of interfacing bar utilized The mathematical model appeared in the past section is discretized utilizing tetrahedral elements. (Figure 1) These components are chosen in view of their capacity to catch the calculation of any intricate model. Since this model is of different shapes and sizes, a tetra component of the primary request is chosen. The wrench was isolated into two parts in the mathematical model and the equivalent has been kept up in the FE



Finite Element model of associating bar

4. CALCULATION AND VALUES

Engine Capacity : 2967 cc

Power developed : 232 hp (173 kW) Torque developed : 300 Nm at 4500 rpm Stroke : 79.5 mm Bore : 89 mm Compression ratio : 10:1

The Forces following up on the cylinder end of the associating bar is given by the condition,

$$\text{Force} = \text{Gas force} - \text{Inertial force} \dots\dots\dots (1)$$

Where, Gas Force = Pressure X Cylinder bore area $\dots\dots\dots (2)$

$$\text{Inertial Force} = m_p \times a_p \dots\dots\dots(3)$$

$$a_p = r \omega^2 \cos \theta + \cos 2\theta n \dots\dots\dots (4)$$

Where, r = Wrench range ω = precise speed θ = Crank plot (For most extreme force, it tends to be expected that the wrench edge will be 0° or 360°) The mean powerful weight inside the chamber can be determined by utilizing the beneath recipe.

$$\text{Force (P)} = P_m \times L \times A \times N \dots\dots\dots (5)$$

Where, P_m = Mean effective pressure (MPa) L = Stroke length (m) A = Area of the cylinder (m^2) N = Speed of the engine (RPM) Angular velocity = $\frac{\pi D N}{60}$

Where, D = Diameter of the crankshaft (m) N = Speed of the engine (RPM)

Or

$$P_m = \frac{173 \times 10^3 \times 60 \times 0.0795 \times 0.006221 \times 4500}{4663988.916} \text{ N/m}^2$$

$$= 4.6 \text{ MPa} = 46 \text{ bar}$$

$$\text{Gas Force} = 4.6 \times \pi \times 89^2 \times 10^{-3} \times 2 \times 10^6 \times 4 = 28.621 \text{ Kn}$$

$$a_p = 39.75 \times 10^{-3} \times 18.73172 = 13.95 \text{ m/s}^2$$

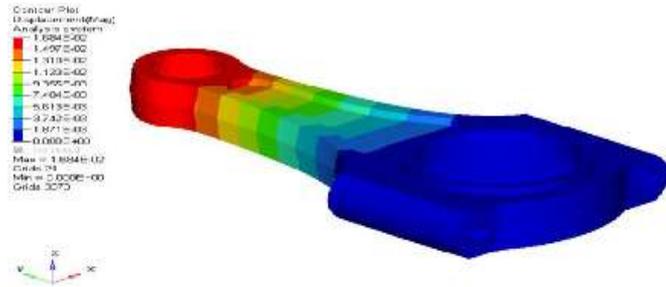
Inertia force = $2.507 \times 13.95 = 35 \text{ N}$ Forces acting on the connecting rod small end = Gas force – Inertial force

$$= 28621 - 35 = 28586 \text{ N}$$

5. RESULTS AND DISCUSSION

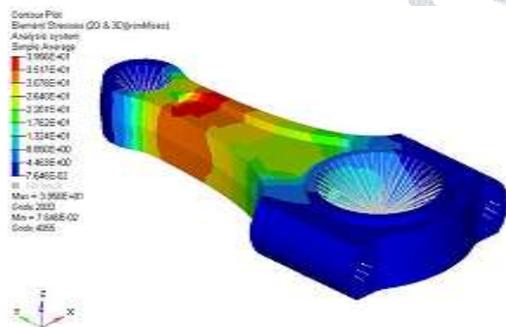
5.1 BUCKLING ANALYSIS RESULTS

The investigation was run for the previously mentioned FE Model with the heaps and limit conditions joined to it. The accompanying figures give the outcomes acquired from both the static examination (Displacement and Stresses) and clasp investigation (Buckling mode)..



. Displacement plot

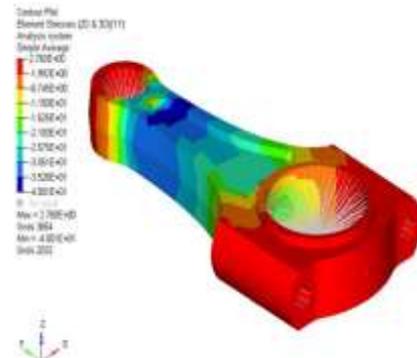
Figure above shows the displacement for the selected connecting rod under the loads applied. It is clear from the above figure that the maximum displacement occurs on the piston end at a value of 0.176 mm and minimum displacement occurs on the crank end at a value of 0 mm.



Elemental stress plot

Figure above shows the Von Mises pressure plot for the chose associating pole under the heaps applied. It is obvious from the above figure that the shank is exposed to a greatest worry close to the cylinder end at an estimation of 414.34 MPa. This worth is a lot of not exactly the yield quality of the material and consequently it can be said that the connecting bar is sheltered

under the applied load value which are measured on ground of the pressure created is well inside the greatest permissible anxiety of 468.85 MPa. This worth is acquired by considering a factor of security of 2 for produced steel which has a definitive quality of 937.7 MPa



Essential pressure plot in Y-heading

Figure shows a pressure plot in the Y-heading of the associating pole for the applied burdens. It very well may be seen that cylinder end and the wrench end of the interfacing bar shows the improvement of worry to a greatest estimation of 28.91 MPa and the remainder of the associating bar falls under the scope of - 70.65 MPa and - 419.1 MPa. The negative sign demonstrates the created of worry in the negative Y-bearing

6. Conclusion

The model of an interfacing bar was created, discretizes and broke down. The outcomes are arranged and introduced in the past parts. From the outcomes it tends to be reasoned that, The dislodging plot shows a tiny worth which doesn't influence the exhibition of the connecting rod. The linear static examination of the connecting rod shows that the pressure created in the model is inside as far as possible or greatest permissible pressure. The stress plots in X, Y and Z headings show that The most extreme pressure is created along the hub of the connecting bar which is expected to the load being applied along the pivot. The shear pressure plot shows that the most extreme shear pressure is developed in the I-segment of the interfacing pole which is additionally inside as far as possible.

The clasp investigation gives the clasp factor more prominent than 1 and thus

it can be concluded that the connecting pole can withstand the load applied.

7. References

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