

# A Theoretical Ponder on the Impact of Different Motor Working Parameters on Sediment Arrangement and Measuring in Diesel Motors: An Investigation

Sumit Kanchan

School of Mechanical Engineering, Lovely Professional University, Phagwara-144411, Punjab, India.

## Abstract

Diesel motors have included a striking spot within the field of traveler cars due to its consistent advancement close designing clean discuss. This survey summarizes the advance on distributed writing with respect to the impact of different motor equipment and working imperatives on sediment creation and its result on motor performance. This work diagrams the method included behind the arrangement of sediment in barrel or within the deplete. In line, the result of motor plan and working imperatives like speed, stack, combustion chamber plan, admissions temperature and “pressure, infusion weight, infusion timing, greasing up oil, and fuel on sediment creation is broadly surveyed. Besides, the think about of result of Debilitate Gas Distribution (EGR) on combustion characteristics, emanations, stores, wear and oxidative reactivity of diesel sediment outflow is examined. Taking after, we did a comprehensive rundown of the work on the adequacy of motor working parameters on sediment lessening. To conclude, the brief comparison between results set up by a few agents for impact of distinctive motor working imperatives on sediment creation and measuring is done. We conclude by finding major parameters influencing the sediment execution on motor life.

**Keywords:** Soot formation, Diesel engines, Load, Injection Pressure

## 1.1 Introduction

For virtual end of key poisons from the diesel deplete outflows, advances have been created which makes strides engine’s warm effectiveness, volumetric productivity, fuel economy, speed, control, and execution of after treatment gadgets. After treatment gadgets has been a range of inquire about from numerous decades for nonstop enhancement of their effectiveness. Higher levels of hurtful outflows within the air, influences the human’s wellbeing and climate, straightforwardly or by implication. Diesel deplete outflows basically incorporate CO, CO<sub>2</sub>, H<sub>2</sub>O, particulate matter, HC and NO<sub>x</sub>, between which NO<sub>x</sub> at that point particulate outflows are of incredible concerns for their sick impacts on wellbeing and climate.

The particulates matter primarily comprises of the carbon sediment created by the combustion handle. Tests performed have appeared that particulate outflows result from both fragmented combustion handle and greasing up oil [1]. Huge volumes of sediment gotten discharges from the debilitate, rest mixes with greasing up oil within the crankcase. Defilement of greasing up oil leads to oil thickening, in this manner giving birth to issues like motor wear, diminished lubricity, execution corruption and pumping issues [2].

Sediment can begin from diverse sources like in-cylinder, flares, debilitate etc., and is famously known as in-cylinder sediment, fly sediment and debilitate sediment separately. Sediment, primarily contains of sulfur, hydrogen, carbon, oxygen and nitrogen in disparate rate. Carbon (80-90%) has most elevated substance while sulfur (1%-2%) is lightest. The hydrogen substance of around 1% by weight is due to the experimental equation C<sub>8</sub>H. By the by, they all concentrate at the sediment surface and gives extremity to its particles [4].

The influence of various physical operating parameters and engines hardware designs on soot behaviour have been widely studied by many researchers [5-9].

The ponders conclude that increment within the levels of particulate matter (primarily sediment) comes about in more wear of basic motor parts such as cylinder ring crevices, barrel liner, cam nose, rocker arm tip, valve direct, valve stem etc. Diverse wear components were proposed by diverse scholars [10, 11] among which adsorption, erosion and scraped area were vital. With adsorption and erosion takes on the surface, scraped area takes after a three-body wear prepare in which two bodies incorporate the two surfaces and third being the sediment molecule caught in between two interferometer bodies. Anti-wear added substances were included to the greasing up oil to diminish the impacts caused due to oil thickening [12]. Ponders concerning the impact of stack [13, 14], infusion weight, infusion timing, powers, greasing up oil, added substances, numerous Infusions, admissions discuss weight and temperature, water emulsifiers, combustion chamber shape and their geometry, assistant discuss supply, whirl and speed etc., on sediment conduct have

been distributed [13-17]. The impact of these parameters on sediment conduct and motor execution is broadly examined in this paper.

### Structure

Diesel sediment structure is pondered by Donnet in detail [4]. Fig. 1 appears the diesel sediment organized itself in chain-like agglomerates and accomplish various hundred nanometres in estimate. These collected circular or nearly-spherical units, are known as foremost sediment particles. These contain 105-106 C-atoms, variable among 10 and 80 nm, but is ordinarily mid-15 and 50 nm in size. The think about of structure and substructure of sediment particles beneath distinctive combustion sources has been examined utilizing Transmission Electron Microscopy (TEM) and Tall- Determination Transmission Electron Spectroscopy (HRTEM). The carbon molecules within the central sediment particles are swarmed in hexagonal face-centred (Fig. 1) cluster, as platelets.

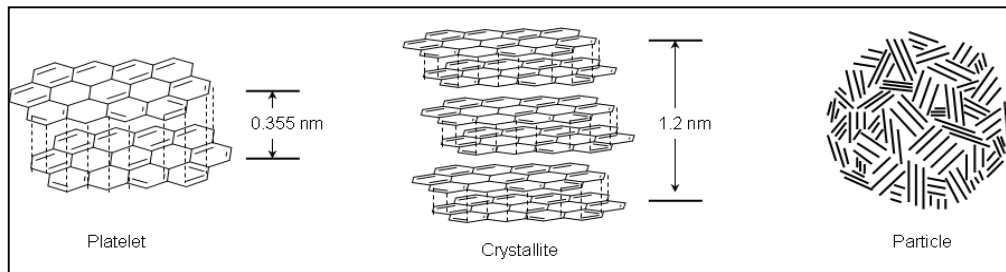


Fig. 1: Primary carbon-particle structure [15]

### 1.3. Influence of engine operating parameters on soot formation

The impact of motor plan and working limitations like speed, stack, combustion chamber plan, admissions temperature and “pressure, infusion timing, infusion weight, greasing up oil, and fuel on sediment creation are critical. These are summarized as,

#### Injection Pressure:

Alteration in infusion weight have a considerable result on normal sediment molecule estimate, channel smoke number (FSN) esteem, particulate matter, gathering of sediment molecule and NO<sub>x</sub> values. Endeavours were made to assess the impact of infusion weight on over factors [19, 20].

#### Influence of injection pressure on filter smoke number

Tests performed by changing the infusion weight to 190 bar from 240 bar, discretely at 1200 rpm on turbocharged motor “shows that as the infusion weight diminishes the sum of channel smoke number increments. Tests conducted appeared that as the infusion weight is expanded FSN values diminishes. Infusion weight utilized amid this consider was 240 bar, 220 bar and 190 bars separately as summarized in table 1. This nature was credited to diminish within the esteem of cruel viable sediment molecule measure diminishes as infusion weight increments subsequently coming about in diminished sum of FSN values and sediment. It is seen that FSN values changes nearly directly with the increment in infusion weight.

Table 1: Result of injection pressure on load & FSN.

Injection pressure values	Speed (rpm)	Load (Nm)	Fuel Consumption (kg/hr.)	FSN
240	1200	295	8.95	3.25
220	1200	297	9.10	3.40
190	1200	301	9.18	3.51

#### i. Effect of Injection Pressure on Mean Particle Size of Soot

Consider performed by Mirza markovic [18], it is set up that the estimate of the agglomerates and chain length of sediment particles diminishes as infusion weight is expanded, likely diminishing number of nanoparticles (sediment estimate) within the agglomerates leads to that result as appeared in Fig. 2.

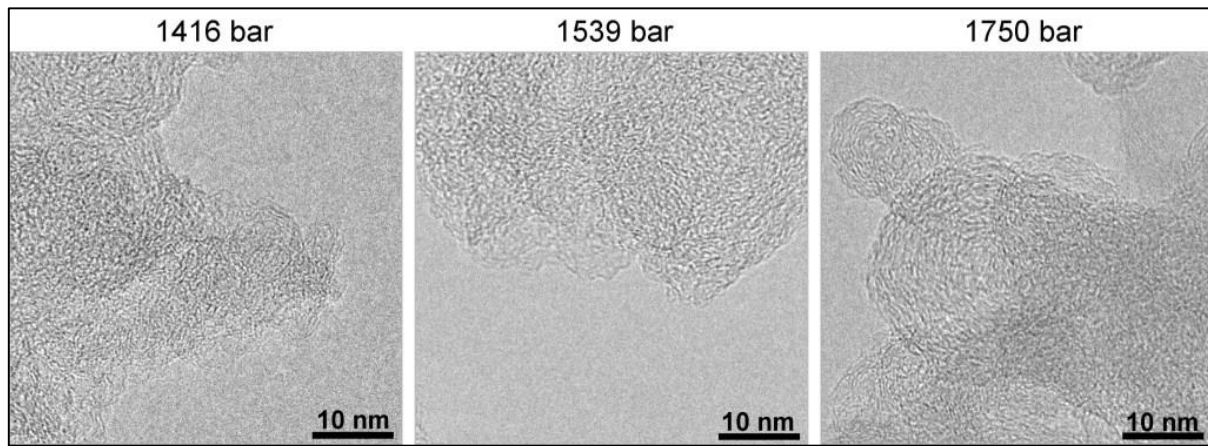


Fig. 2: Effect of injection pressure on mean effective pressure size.

## ii. Effect of Injection Pressure on Soot

Impact of infusion weight at 75% stack on structure of sediment [20] is illustrated by explore conducted on Euro V diesel motor at MAN Nuremberg. At each weight the TEM pictures were taken which appeared impact of infusion weight on structure of sediment. Test was conducted at distinctive motor speeds and changing infusion weight and EGR as appeared within the table 2 [18, 19, and 20].

Operating parameters	Test 1	Test 2	Test 3
Engine speed, rpm	1199	1201	1199
Mass flow rate (diesel) (kg/h)	41.3	41.7	40.8
Injection pressure (bar)	1416	1539	1750
FSN	0.10	0.07	0.06

Table. 2. Experimental data used to show the effect of injection pressure on soot structure and NO<sub>x</sub> [18, 19, 20, and 35]

The changes watched at distinctive infusion weights can be summarized as: At 1416 bar- Turbostratic gatherings comprising a tall volume of muscularly twisted and chaotic graphitic lamellae were detected.” At 1539 bar- More requesting sediment particles were observed. At 1750 bar- Fullerene like structure (closed empty cages comprising of carbon molecules interconnected in pentagonal and hexagonal rings) or onion formed structures were shaped. It was built up that with rise in infusion weight the turbostratic structures of sediment particles changes to onion formed closed structures subsequently picking up stability.

## iii. Injection pressure effect on NO<sub>x</sub>

Infusion weight moreover have an unfavourable impact on NO<sub>x</sub> arrangement. Considers affirmed that as the infusion weight increments the sum of NO<sub>x</sub> too increments. This is often ascribed to the sum of sediment produced at a few infusion weights. At lower infusion weight sum of sediment produced is more hence restricting the arrangement of NO<sub>x</sub>. “Similarly, with the rise in infusion weight, the sum of sediment created decays and the esteem of NO<sub>x</sub> rises.

### Impact of nitrogen oxides (NO, NO<sub>2</sub>, N<sub>2</sub>O) on the formation of soot

Nitrogen oxide can influence the sediment emanation when show in recalculating blend. To examine this marvels Maria et al [67] performed pyrolysis tests of C<sub>2</sub>H<sub>4</sub> (ethylene) show at 30000 ppm; at concentration of distinctive nitrogen oxide as 0, 500, 1000, 5000 & 12000 ppm expressed that, at concentration 12000 ppm of NO<sub>2</sub> sediment outflow is lower than at without nitrogen oxide. Concentration of N<sub>2</sub>O is less than 5000 ppm because it given great condition for more sediment outflow but at 12000 ppm sediment emanation diminished

### b. Influence of fuel injection pressure on diesel number distribution and particulate size

Avinash Kumar Agarwal et al [62] performed experiments on three different pressure (300, 500 and 700 bar) and at 4 changed injection timing for finding the consequence of injection pressure on diesel particulate size and number distribution. It was established that particulate size number concentration rises with growing engine load. Further, it reduces with rise in fuel injection pressure.

#### 1.3.1 Effect of Fuel on Soot

It is the fuel properties which influences the soot formation and not fuel as a whole. Cetane number and additives in the fuel affects the soot formation directly or indirectly. Various researches [21, 22, 23, 26] have been done in the past which explore the effect of properties of fuel on soot formation. These can be summarized as follows:

##### i. Cetane Number.

Cetane number characterizes the start quality of the fuel [1]. It is characterized by mixes of two immaculate hydrocarbons (n-hexadecane and heptamethylnonane) as reference powers. Inappropriate cetane number influences the combustion timing coming about in delay. In this delay period the fuel auto lights, in this way called auto start delay.



Higher the start delay higher will be the fuel devoured. Higher the fuel devoured more will the temperature of combustion, which is specifically coupled with increment in diesel sediment [1] In this way in arrange to diminish sediment, fuel with higher cetane number ought to be utilized. With higher cetane number the fire moves upward, closer to the injector, in this way auto start quality happens early [12]. With early auto start delay, littler particles were delivered in this way getting oxidized promptly. This comes about in less sum of diesel sediment.

“For deciding the impact of cetane number on sediment arrangement, 3 powers having three CN at a few infusions and in-cylinder weight were tried. A recognizable impact on the measured sediment volume division of cetane number was watched. A lessening of the sediment volume division was recognizable from the begin of test, for higher cetane numbers (24). Junheng Liu et al. [65-66] did tests to look at the result of fuel with progressed infusion timing, on 6-cylinder turbocharged motor by utilizing diesel and methanol as a fuel. It was concluded that by developing methanol mix and at progressing infusion timing increment the top barrel weight subsequently expanding crest warm discharge rate and sediment emanations. Assist M. Storch et al. [61] performed tests to look at the impact of ethanol mixing (E20 by vol) on combustion and sediment arrangement. It was detailed that sediment radiance escalated is more as compared to isooctane.

#### **Addition of Additives to Fuel:**

Added substances were included in arrange to expand the life of moving parts working beneath changing conditions of speed, weight and temperature. Sediment produced from distinctive sources like in-cylinder sediment, divider testimony sediment, diesel deplete sediment, fly sediment etc., got to be optimized for legitimate working of the motor and to attain more tightly contamination orders. Hence, fuel added substances such as ethanol, ethylene glycols dimethyl ether, succinimide (dispersant), polyethylene glycol dinitrate, nitro-methane and nitro-compound blend were included in arrange to diminish the in-cylinder sediment shaped amid operation. Different ponders have been done appearing the impact of distinctive fuel added substances on the in-cylinder sediment arrangement [20,25] but ethanol containing powers is considered to have the most noteworthy potential for diminishment of sediment [26]. The ethanol added substance, at 10 % by mass, diminishes jet-soot by 15%, and brings down wall-soot by 30-40%.

#### **Impact of Injection Timing on Soot Structure**

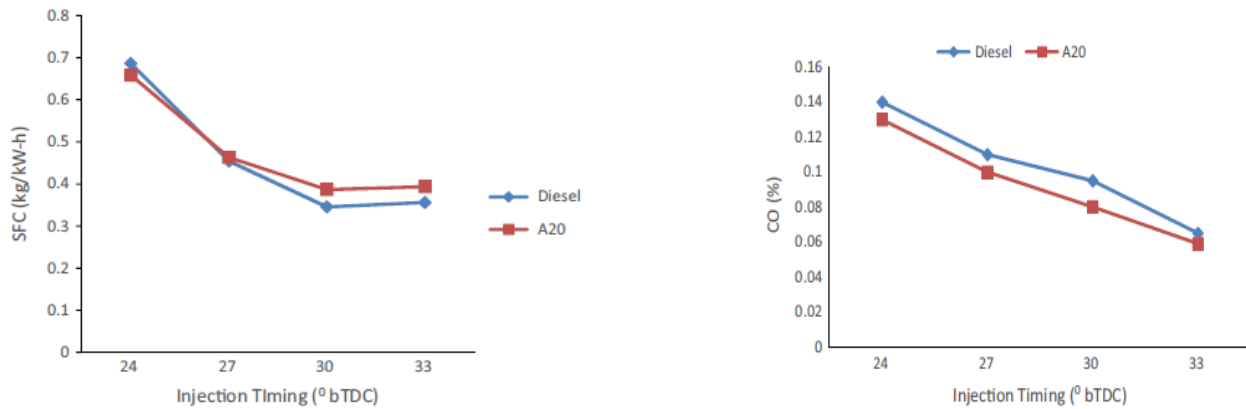
The concept of low temperature combustion is widely known. This describes the synchronized decrease in PM and NO<sub>x</sub> by keeping the flame temperature restricted to stages where the soot creation rate is lesser [27 - 32]. Variation in injection timing effects the engine characteristics like squish and ignition delay [33, 50 - 58].

The impacts of development and hindered infusion on sediment arrangement, sediment distance across and molecule number estimate dispersion were inspected. It was built up that with development infusion timing, the early admissions discuss temperature and weight are brought down subsequently expanding the start delay. With deferred infusion timing, admissions discuss weight and temperature are firstly somewhat more but as the delay continues it diminishes [34].

Infusion timing and infusion weight has importance impact on outflow of sediment and NO<sub>x</sub>. To look at the result of infusion weight and timing, Nader Raeie et al. [60] did tests on six assorted infusion weight from 270 bar to 1010 bar (BTDC & ATDC) and built up that early infusion makes lesser sediment and more NO<sub>x</sub> emanation in late infusion.

To review the result of infusion timing and compression proportion on particular fuel utilization (SFC), brake warm productivity (Bth) and outflows of Smoke, NO<sub>x</sub>, CO, HC, Senthil Ramalingam et al. [69] performed strings of tests by utilizing Annona methyl ester as a fuel. Exploratory condition executed a compression proportion (19.5) and infusion timing (30o BTDC) in their consider. It was set up that the collective rise of compression proportion and infusion timing rises the BTE and diminishes SFC whereas having lesser outflows of sediment. Essentially, examination was done on finding the result of infusion timing on diesel motor with a fuel blend.

For this, Arun kumar Wamankar et al [55] performed experiments at five injection timing (20, 21, 23, 24.5 & 26<sup>o</sup>CA BTDC) and synthetic fuel (comprising of 20% black carbon and 80% diesel) and stated that at 23<sup>o</sup> CA main injection and at 26<sup>o</sup> CA BTDC & 24.5<sup>o</sup> CA BTDC advanced injection timing BTE increased by around 6.4% and 2.2% respectively, while the fuel consumption decreased by about 11.9% and 8.6% compared to OEM injection timing as shown in Fig. 3.



**Fig. 3.** Effect of injection timing for diesel and blend on SFC and CO emission.

### Soot particle diameter

At low motor loads and with progressed Start of Infusion (4o CA ATDC to 4o CA BTDC) sediment unit breadth measure diminishes from 25.9 to 17.5 nm. At tall motor loads and with progressed Begin of Infusion (4o CA ATDC to 3o CA BTDC) sediment molecule distance across diminishes from 28.4mm to 21.6 nm.

### Particle number size distribution:

At low loads and advanced Start of Injection, slight impact on soot particle number size distribution.

At high loads and advanced Start of Injection, significant amount of reduction (62nm to 53nm) were noticed.

### Engine load impact on diesel soot.

It is well known that as stack increments the sum of fuel infused increments, coming about in increment in temperature giving adequate environment for beginning sediment arrangement. To find out the result of stack on diesel sediment molecule Virtanen et al. [35] performed tests on a traveller car vehicle devouring both EGR and oxidation catalyst and on a city transport vehicle devouring as it were oxidation catalyst. Fractal measurement was utilized to characterize the agglomerate structure as well as molecule mass, as a work of portability measure [36, 37]. It was concluded that for both traveller and city transport vehicles the fractal measurement of molecule diminishes and width of sediment dissemination increments with increment in stack. The molecule estimate esteem lies between 2.6 to 2.8 mm depending on motor load.”

Srivastava et al [38] performed tests on diverse loads taking 0kW, 3kW and 5kW individually at steady speed (1500 rpm) and measured the measure of a molecule utilizing Motor Debilitate Molecule Sizer (EEPS). It was found that measure and mass of sediment molecule rises with rise within the motor stack, may be due to rise in fuel infused, hence expanding the combustion chamber temperature. Too, littler molecule mass compared to bigger molecule mass have higher surface zone per unit mass and more unsafe for human wellbeing since it gives expansive surface zone for retention of poison. It was too found that with increment in motor stack, surface area of the molecule decreases. Kittelson et al. [39] reported that surface area could be a work of person cores within the agglomerates instead of agglomerates size.

### Lubricating oil additive on diesel particulate

Clague et al [4] compared conventional oil with diverse kind of present day added substance included oil on the premise of physical and chemical properties. To discover the impact of grease up oil on morphology, measure dispersion and nanostructure. Wang et al [47] performed tests on four –cylinder turbocharged diesel motor at 1200rpm and 2400rpm beneath consistent stack and detailed that cruel breadth of essential molecule for non-additive fuel expanded 22.25nm to 24.99nm whereas for mixed fuel values are diminished 24.18nm to 20.75 when speed expanded from 1200 rpm to 2000rpm. Fractal measurements of total and division remove of layer both appear inclination to extend after added substance included in oil whereas periphery length decreases.

### 1.3.6 Multiple injection timing

Multiple injection is one of the best strategies for soot reduction. To investigate the effect of multiple injection timing on soot emission. Hyun Kyu Suh [53] performed experiments and concluded that in multiple injection combustion, more CO formation and less HC emission.

### 1.3.7 Injection timing on Pre-Heating

Pilot fuel injection timing and intake temperature are the two significant parameter in dual fuel (Diesel–methanol) which influence the combustion characteristics and soot emission .To examine the result of intake pre heating and injection, Chunde Yao et al [56] performed experiments on methanol fumigated diesel engine at five different injection timing (-17.4,-11.4,-7.4,-1.4,4.6 °CA ATDC) and three different pre heating temperature(35,75,105°C) and concluded that As

rise in the intake air temperature notably reduced the combustion delay and BTE at low load is better by 7.3% by rising intake air temperature.

### 1.3.8 Soot in Oil

To explore the characteristic of sediment in oil. A. La Rocca [58] performed tests on 4-cylinder light obligation Euro IV @ 1600-3700 rpm and torque at 30-120 Nm. Advance after 30-hour motor operation sediment gotten from oil and watched by TEM and found that cruel skeleton length, width and fractal measurement were 153nm ,59nm and 144 separately. Foremost sediment molecule watched as circular shape whose normal breadth were 36nm. Further to explore the effect of fuel on sediment emanation, Chongming Wang et al [59] did tests on single barrel GDI motor at 1500 rpm , IMEP shifted between 3.5-8.5 bar and infusion weight expanded from 50 bar to 150 bar and compared between two powers (Gasoline and ethanol) and found that when ethanol utilized as a fuel sediment mass emanation lower but sediment molecule number were higher than that gasoline and when infusion weight expanded it moved forward molecule emanation with gasoline fuel but when ethanol utilized as a fuel and infusion weight improved from 50 bar to 150 bar particle mass reduced by 22% and particle number reduced by 78% [60]

### 1.3.9 Effect on Oxygen Index

To study the effect of oxygen Index on reaction geometry, soot creation and temperature, in ethylene inverse diffusion flame (IDF), F. Escudero et al [61], conduct experimental study by vary the oxygen index from 21% to 37% with constant volumetric ethylene flow rate and measured flame height by emission of CH radical and found that with increasing oxygen index from 21%-37% reaction zone decreased 22.3nm -21.4nm and soot temperature existed between 1800-2500K .With increasing the soot temperature soot volume fraction increases as oxygen index increased from 21-37%.

### 1.4 Effect of Exhaust Gas Recirculation (EGR) on combustion performance.

Analysts are working ceaselessly to update the innovations so that the diesel debilitate outflows can be decreased, fuel utilization, and to extend fuel economy. As a result, later patterns showed remarkable increment within the deals of diesel cars [29, 30], owing to extend in warm productivity and fuel economy without compromising with the control. Motor producers are working on making their motors more productive, on other side to control the emanations from the vehicles, the administrative outflows standards have been fixed.

In case of diesel motors, primary emanations incorporate NO<sub>x</sub> and particulates from the debilitate. For the lessening of NO<sub>x</sub> from both diesel and gasoline motors, deplete gas distribution has demonstrated to be the foremost critical strategy [31, 32]. Exhaust gas distribution strategy utilizes the admissions of portion of the deplete gas back into the admissions complex exchanging the break even with volume of new discuss. It blends with the new discuss within the admissions complex. Subsequently, it brings down the sum of oxygen concentration and decrease fire temperature subsequently coming about within the decreased NO<sub>x</sub> emanation [33]. But in case debilitate gas distribution has positive side it has negative side as well. With the presentation of the exhaust gas distribution, the sediment substance increments within the greasing up oil driving to extend in thickness of the oil [33]. Publishes studies revealed that the polluted lubricating oil effects the wear of engine components such as cam noses, piston rings, crosshead assembly etc. [32]. It was found that the significant amount of wear occurred at cam nose engine component due to the abrasive action.

### There are two types of EGR employed today: 1. Hot EGR and 2. Cold EGR.

In hot EGR, hot debilitate gas mixes with the new admissions discuss. The blend due to a tall temperature abbreviates the start delay in this manner moving forward the warm productivity. In cold EGR, portion of debilitate gasses some time recently blending with new discuss, is made to cool subsequently diminishing its temp. In this way, the blend of new charge and cold EGR rises the charge thickness in this manner making strides volumetric effectiveness, driving to reducing of NO<sub>x</sub> outflow from the deplete.

Exhaust gas recirculation, effect the physical properties of the soot as found by Xiling et al [34]. They compared two samples of the soot at 0% and 20% EGR levels, with soot samples taken from DDC/VM motori 2.5; 4-cylinder, turbo charged, CRDi, DI, engine running at 1600 rpm and 60 lb-ft of torque. Table 3 summaries the effect of different parameters on soot performance with engine employed with and without EGR.

**Table 3:** Conclusion from the published study showing the effects of different EGR levels on different engine parameters [34, 65,66]

Effect on different parameters:	With EGR (20%)	Without EGR (0%)
Soot reactivity.	Increases.	Slight increase until 18% conversion: due to evaluation of residual VOF. 18% to 40 % conversion, No significant change.

Structural analysis of soot.	Interspacing between crystallite increases. Crystallite Height decreases. Crystallite width decreases.	<b>Lower</b> as compared to with EGR values. <b>Higher</b> as compared to with EGR values. <b>Higher</b> as compared to with EGR values.
Characterization of inactive sites.	Increase in active sites, thus increase in soot reactivity.	Lower as compared to with EGR values.
Morphological evaluation.	Shows dual burning oxidation process (internal + external)	Shows only external burning oxidation process.

The soot reactivity increases due to introduction of the EGR was attributed to rise in specific rate of soot oxidation. In structural analysis the increase in the interlayer spacing of crystallites was attributed to particles highly disordered nature.

The **EGR rate** can be calculated by any one of the following equations:

- $EGR(\%) = \frac{M_{egr}}{M_{intake}} \times 100;$
- $EGR(\%) = \frac{(CO2)_{int} - (CO2)_{atm}}{(CO2)_{ext} - (CO2)_{atm}}$ ; based on NDIR CO<sub>2</sub> measurement technique,
- $EGR(\%) = \frac{V_{egr}}{V_{egr} + V_{air}} \times 100;$

Debitate gas distribution moreover impacts the corrosive substance of the greasing up oil TAN. Increment in corrosive number of the greasing up oil due to EGR, was ascribed to the increment in sulphuric corrosive due to expansion of debitate gas into the admissions complex [35, 64]. Hence, increment in corrosive substance, increment the destructive wear of the greased-up parts [32]. Too, straight relationship was found with sediment substance and TAN on wear i.e., as sediment substance and oil corrosive substance increments, the wear on basic motor parts increments.

At higher loads, NO<sub>x</sub> decreases with increment rate of EGR, breaking down execution and emanation, while at low loads, NO<sub>x</sub> decreases with increment rate of EGR without debasing execution and emanations, subsequently higher rates of EGR were utilized at lesser loads. Moreover, at lesser loads warm effectiveness and BSFC diminishes. As stack increments it creates more smoke due to alarm of oxygen in diesel motors [30].

Separated from EGR a few other strategies were moreover received in arrange to diminish NO<sub>x</sub> [30]. Cetane number moving forward added substances, hindered infusion and water infusion are a few of them. Cetane number moving forward added substances were found to decrease NO<sub>x</sub> insulant. Hindered infusion timing increments the fuel utilization, smoke, diminished control and increment HC emanations and in this way the thought of utilizing impeded infusion timing for NO<sub>x</sub> decrease was dropped. In water infusion partitioned weight of water tank increments the weight of the framework, moreover, troublesome to support water at a wanted temperature amid cold conditions.

Table 4. abridges the result of distinctive working parameters on motor execution utilized with EGR.

**Table 4.** A brief summary of result of different working parameters on different engine performance employed with EGR. [10, 11, 29-34, 59-63]

Effect on different parameters	Effects (with EGR)
At low Load	<ul style="list-style-type: none"> <li>• Increase in thermal efficiency.</li> <li>• Decrease in BSFC</li> <li>• Reduces NO<sub>x</sub> without deteriorating performance and emission (increasing EGR rate)</li> </ul>
At high loads	<ul style="list-style-type: none"> <li>• Thermal efficiency and BSFC remains approx. same.</li> <li>• Reduces NO<sub>x</sub>, deteriorating performance and emission (increasing EGR rate).</li> </ul>
Soot particulate	<ul style="list-style-type: none"> <li>• Increases (7-12% compared to 4% without EGR).</li> </ul>
Total Acid Number (TAN)	<ul style="list-style-type: none"> <li>• Increases by two to three times.</li> </ul>

For assessing particulate matter emanation from low temperature combustion and routine combustion, Yongjin Jung et al. [66] did tests on single barrel diesel motor whose compression proportion was 17.4 and steady speed 1200 by utilizing TGA and TEM and concluded that proportion of carbon to hydrogen in case of low temperature combustion were 3.384 and for customary combustion it was 6.74 and measure of sediment molecule at low combustion were less than routine combustion.

**Conclusion**

1. With the hypothetical examination been worn out this consider for finding the effect of a few motor working parameters on the sediment arrangement and sizing, numerous comprehensive conclusions may be established. 1. Soot molecule measure expanded with increment the stack. The sediment estimates changes from 40–50 nm (nanometre) at no stack; 60–70 nm at full load.



2. 2. In the sediment arrangement at 0% EGR, nucleation mode overwhelmed and at late infusions aggregation mode overwhelmed the arrangement prepare. Besides, when engine operated with EGR, sediment substance is approx. 5% higher than without EGR.
3. 3. It is clear that particulate matter mass and mass outflow increments with progress infusion timing. Advance Sediment emanation declined by 38.6% @ 30% methanol substitution and HC and CO emanations surge by 90.6% and 32.7%, individually for 30% methanol substitution.
4. It is clear that at progressed infusion smoke emanation set up to be lower by 13.5% while at Impeded Infusion sediment emanation set up to be lower by 72%
5. Moreover at 5.5oCA ATDC, sediment built up to be diminished. Encourage, at 300CA BTDC, appeared lower outflows of sediment as when compared with standard infusion timing of 27oCA BTDC.
6. It is set up that with increment in Sauter cruel breadth (SMD) vaporization of fuel beads decreases.
7. At higher infusion weight and development infusion timing particulate number concentration found to be decreased. Additionally, at lower infusion weights, PM concentration to begin with rises, at that point decreases with impeded infusion timings.
8. For ethanol mixing, E20 appeared more grounded sediment glow than isoctane. 9. For oxygen list, sediment volume division rises with developing OI.

### Nomenclature

Symbol	Description	Unit
N	Engine speed	rpm
T	Torque	Nm
A	Alpha	-
T	Time	sec
P	Density	kg m <sup>-3</sup>
M	dynamic viscosity	kg s <sup>-1</sup> -m
<i>Megr</i>	Mass of exhaust gas inducted in intake manifold through EGR	kg
<i>Vegr</i>	Volume of recirculating exhaust gas	cm <sup>3</sup>
<i>Vair</i>	Volume of fresh air entered in the intake manifold	cm <sup>3</sup>
<i>(CO2)int</i>	Amount of CO <sub>2</sub> entered in the intake manifold	ppm
<i>(CO2)atm</i>	Amount of CO <sub>2</sub> in the atmosphere	ppm
<i>(CO2)ext</i>	Amount of CO <sub>2</sub> in the exhaust	ppm

### Abbreviations

BTE	Brake Thermal Efficiency	FSN	Filter Smoke Number
BSFC	Brake Specific Fuel Consumption	FIP	Fuel Injection Pump
PAH	Polycyclic Aromatic Hydrocarbons	HRTEM	High resolution transmission electron microscope
C <sub>2</sub> H <sub>2</sub>	Acetylene	ZDDP	Zinc dialkyl dithiophosphate
ATDC	After Top Dead Centre	CO	Carbon Monoxide
BTDC	Before Top Dead Centre	CO <sub>2</sub>	Carbon dioxide
TEM	transmission electron microscopy	NO <sub>x</sub>	Nitrogen oxide
TGA	Thermogravimetric analysis	SO	Sulphur oxide
EGR	Exhaust Gas Recirculation	WOT	Wide Open Throttle
NDIR	Non-Destructive Infrared	CI	Compression ignition
SMD	Sauter Mean Diameter	EOT	End of test
DICI	Direct Injection Compression Ignition	TAN	Total acid number
KV	Kinematic Viscosity	HC	Hydrocarbon
T <sub>ext</sub>	Temperature of Exhaust	SEC	Spherical Elemental Carbon
TWI	Temperature of Water Inlet	EEPS	Engine Exhaust Particle Sizer.
TWO	Temperature of Water Outlet	IMEP	Indicated Mean Effective Pressure
CSA	Compressed air supply	BMEP	Brake Mean Effective Pressure

### References

- [1]. Heywood, John B. Internal combustion engine fundamentals. Vol. 930. New York: McGraw-Hill, 1988. Pp. 70-71
- [2]. Higgins, B. and Siebers, D., "Measurement of the Flame Lift-Off Location on DI Diesel Sprays Using OH Chemiluminescence," SAE international Technical Paper 2001-01-0918.
- [3]. Clague ADH, Donnet JB, Wang TK, Peng JCM. A comparison of diesel engine soot with carbon black. Carbon 1999;37(10):1553–65.
- [4]. S. Antusch, M. Dienwiebel, E. Nold, P. Albers, U. Spicher, M. Scherge "On the tribochemical action of engine soot" Elsevier. Wear 269 pp.1–12, March 2010.
- [5]. C. Esangbedo, A. L. Boehman, J.M. Perez "Characteristics of diesel engine soot that lead to excessive oil thickening" Elsevier. Tribology international 47 pp.194-203, November 2011.



- [6]. M. Diaby, M. Sablier, A. Le Negrate, M. El Fassi, J. Bocquet "Understanding carbonaceous deposit formation resulting from engine oil degradation" Elsevier. Carbon 47 pp. 355-366, October 2008.
- [7]. S. Bensaid, D.L. Marchisio, N. Russo, D. Fino "Experimental investigation of soot deposition in diesel particulate filters" Elsevier. Catalysis today 147S pp. S295- S300, August 2009.
- [8]. K H Lee, J W Chung, B S Kim, S K Kim, "Investigation of Soot Formation in a D.I. Diesel Engine by Using Laser Induced Scattering and Laser Induced Incandescence" KSME International Journal, VoL 18 No. 7, pp. 1169~1176 2004
- [9]. S George, S Balla, M Gautam, "Effect of diesel soot contaminated oil on engine wear" Elsevier. Wear 262 pp. 1113-1122, December 2006.
- [10]. M Gautam, K Chitoor, M Durbha, J C. Summers, "Effect of diesel soot contaminated oil on engine wear - investigation of novel oil formulations" Elsevier. Tribology international 32 pp. 687-699, October 1999
- [11]. M P. B. Musculus, J Dietz, "Effects of Diesel Fuel Combustion-Modifier Additives on In-Cylinder Soot Formation in a Heavy-Duty DI Diesel Engine" SANDIA REPORT, SAND2005-0189. July 2005
- [12]. A. K. Virtanen, J.M. Ristimaki, K.M. Vaaraslathi, J Keskinen, "Effect of Engine Load on Diesel Soot Particles" Environ. Sci. Technol. 38, pp. 2551-2556, 2004
- [13]. D K Srivastava, A K Agarwal, T Gupta, "Effect of Engine Load on Size and Number Distribution of Particulate Matter Emitted from a Direct Injection Compression Ignition Engine" Aerosol and Air Quality Research, 11, PP.915-920, 2011.
- [14]. R. Prasad, V R Bella, "A Review on Diesel Soot Emission, its Effect and Control", Bulletin of Chemical Reaction Engineering & Catalysis, 5 (2), pp. 69-86, June 2010
- [15]. S George, S Balla, M Gautam, "Effect of diesel soot on lubricant oil viscosity" Elsevier. Tribology international 40, pp. 809-818, September 2006
- [16]. C.D. Rakopoulos, E.G. Giakoumis, D.T. Hountalas, D.C. Rakopoulos, "The Effect of various dynamic, thermodynamic and design parameters on the performance of a turbocharged diesel engine operating under transient load conditions" SAE international, 2004-01-0926.
- [17]. M. Mackovic, "Characterization of soot particles from diesel engines and tin dioxide particles milled in stirred media mills" M. Tech dissertation Department Werkst off wissen schaften (WW7), 2012
- [18]. B Mohan, W Yang, S Chou, "Fuel injection strategies for performance improvement and emissions reduction in compression ignition engines—A review" Elsevier. Renewable and Sustainable Energy Reviews 28 pp. 664-676, September 2013.
- [19]. L M Pickett\* and D L Siebers, "Soot formation in diesel fuel jets near the lift-off length", Sandia National Laboratories, Vol 7, pp. 105-130, 2006
- [20]. Stratakis, G. A., and A. M. Stamatelos. "Thermo gravimetric analysis of soot emitted by a modern diesel engine run on catalyst-doped fuel." *Combustion and Flame* 132.1 (2003): 157-169.
- [21]. Hayashi, Jun, et al. "Effects of fuel droplet size on soot formation in spray flames formed in a laminar counterflow." *Combustion and Flame* 158.12 (2011): 2559-2568.
- [22]. Tree, Dale R., and Kenth I. Svensson. "Soot processes in compression ignition engines." *Progress in Energy and Combustion Science* 33.3 (2007): 272-309.
- [23]. Oger, B. (2012). Soot characterisation in diesel engines using laser-induced incandescence (Doctoral dissertation, University of Brighton).
- [24]. O'Connor, J. and Musculus, M., "Post Injections for Soot Reduction in Diesel Engines: A Review of Current Understanding," SAE Int. J. Engines 6(1):2013, doi:10.4271/2013-01-0917.
- [25]. Souza de Carvalho, Margareth Judith, et al. "Lubricant viscosity and viscosity improver additive effects on diesel fuel economy." *Tribology International* 43.12 (2010): 2298-2302.
- [26]. Kook, Sanghoon, et al. The influence of charge dilution and injection timing on low-temperature diesel combustion and emissions. No. 2005-01-3837. SAE Technical Paper, 2005.
- [27]. Martin, Glen C., et al. Early direct-injection, low-temperature combustion of diesel fuel in an optical engine utilizing a 15-hole, dual-row, narrow-included-angle nozzle. No. 2008-01-2400. SAE Technical Paper, 2008.
- [28]. Benajes, Jesus, et al. Particle size distribution measurements from early to late injection timing low temperature combustion in a heavy duty diesel engine. No. 2010-01-1121. SAE Technical Paper, 2010.
- [29]. Benajes, Jesús, et al. "Increased particle emissions from early fuel injection timing Diesel low temperature combustion." *Fuel* 94 (2012): 184-190.
- [30]. Jacobs, Timothy J., et al. Lean and rich premixed compression ignition combustion in a light-duty diesel engine. No. 2005-01-0166. SAE Technical Paper, 2005.

- [31]. Aoyama, Taro, et al. An experimental study on premixed-charge compression ignition gasoline engine. No. 960081. SAE Technical paper, 1996.
- [32]. Roy, Murari Mohan. "Effect of fuel injection timing and injection pressure on combustion and odorous emissions in DI diesel engines." *Journal of Energy Resources Technology* 131.3 (2009): 032201.
- [33]. Li, Xinling, et al. "Effect of injection timing on particle size distribution from a diesel engine." *Fuel* (2014).
- [34]. Virtanen, Annele KK, et al. "Effect of engine load on diesel soot particles." *Environmental science & technology* 38.9 (2004): 2551-2556.
- [35]. Forrest, S. R.; Witten, T. A. Long-range correlations in smoke particle aggregates. *J. Phys. A: Math. Gen.* 1979, 12, 109-117
- [36]. Rogak, S. N.; Flagan, R. C.; Nguyen, H. V. Mobility and structure of aerosol agglomerates. *Aerosol Sci. Technol.* 1993, 18, 25-47.
- [37]. Suro, J. "Characterization of chemical composition and size of diesel exhaust particulate matter by Iditofms" (2000).
- [38]. Agarwal, Deepak, Shrawan Kumar Singh, and Avinash Kumar Agarwal. "Effect of Exhaust Gas Recirculation (EGR) on performance, emissions, deposits and durability of a constant speed compression ignition engine." *Applied Energy* 88.8 (2011): 2900-2907.
- [39]. Santoro, Robert J. "Soot particle formation in diffusion flames." Fall meeting of the American Chemical Society, Division of Fuel Chemistry. 1987.
- [40]. Shayler, P. J., et al. The influence of pilot and split-main injection parameters on diesel emissions and fuel consumption. No. 2005-01-0375. SAE Technical Paper, 2005.
- [41]. Parrish, Scott E., Gaoming Zhang, and Ronald J. Zink. Liquid and vapor envelopes of sprays from a multi-hole fuel injector operating under closely-spaced double-injection conditions. No. 2012-01-0462. SAE Technical Paper, 2012.
- [42]. Molina, Santiago, et al. A numerical investigation on combustion characteristics with the use of post injection in DI diesel engines. No. 2010-01-1260. SAE Technical Paper, 2010.
- [43]. Desantes, José M., et al. A comprehensive study of diesel combustion and emissions with post-injection. No. 2007-01-0915. SAE Technical Paper, 2007.
- [44]. Han, Zhiyu, et al. Mechanism of soot and NO<sub>x</sub> emission reduction using multiple-injection in a diesel engine. No. 960633. SAE Technical Paper, 1996.
- [45]. Beatrice, C., et al. "Diesel combustion control in common rail engines by new injection strategies." *International Journal of Engine Research* 3.1 (2002): 23-36.
- [46]. Dronniou, Nicolas, et al. Combination of high EGR rates and multiple injection strategies to reduce pollutant emissions. No. 2005-01-3726. SAE Technical Paper, 2005.
- [47]. Barro, Christophe, et al. "Influence of post-injection parameters on soot formation and oxidation in a common-rail-diesel engine using multi-color-pyrometry." ASME 2012 Internal Combustion Engine Division Fall Technical Conference. American Society of Mechanical Engineers, 2012.
- [48]. Chen, S. Kevin. Simultaneous reduction of NO<sub>x</sub> and particulate emissions by using multiple injections in a small diesel engine. No. 2000-01-3084. SAE Technical Paper, 2000.
- [49]. Montgomery, David T., and Rolf D. Reitz. Effects of multiple injections and flexible control of boost and EGR on emissions and fuel consumption of a heavy-duty diesel engine. No. 2001-01-0195. SAE Technical Paper, 2001.
- [50]. Pierpont, D. A., D. T. Montgomery, and Rolf D. Reitz. Reducing particulate and NO<sub>x</sub> using multiple injections and EGR in a DI diesel. No. 950217. SAE Technical Paper, 1995.
- [51]. Ehleskog, Rickard, and Raúl L. Ochoterena. Soot evolution in multiple injection diesel flames. No. 2008-01-2470. SAE Technical Paper, 2008.
- [52]. Shayler, P. J., et al. The influence of pilot and split-main injection parameters on diesel emissions and fuel consumption. No. 2005-01-0375. SAE Technical Paper, 2005.
- [53]. Yang, B., A. M. Mellor, and S. K. Chen. Multiple injections with EGR effects on NO<sub>x</sub> emissions for DI diesel engines analyzed using an engineering model. No. 2002-01-2774. SAE Technical Paper, 2002.
- [54]. Desantes, José María, et al. "A Comprehensive Study of Particle Size Distributions with the Use of PostInjection Strategies in DI Diesel Engines." *Aerosol Science and Technology* 45.10 (2011): 1161-1175.
- [55]. M. Abián, E. Peribáñez, Á. Millera, R. Bilbao, and M. U. Alzueta, "Impact of nitrogen oxides ( NO , NO 2 , N 2 O ) on the formation of soot," *Combust. Flame*, vol. 161, no. 1, pp. 280–287, 2014.

- [56]. N. Raeie, S. Emami, and O. Karimi Sadaghiyani, "Effects of injection timing, before and after top dead center on the propulsion and power in a diesel engine," *Propuls. Power Res.*, vol. 3, no. 2, pp. 59–67, 2014.
- [57]. R. Senthil, R. Silambarasan, and N. Ravichandiran, "Influence of injection timing and compression ratio on performance, emission and combustion characteristics of Annona methyl ester operated diesel engine," *Alexandria Eng. J.*, vol. 54, no. 3, pp. 295–302, 2015.
- [58]. C. Sayin and M. Canakci, "Effects of injection timing on the engine performance and exhaust emissions of a dual-fuel diesel engine," *Energy Convers. Manag.*, vol. 50, no. 1, pp. 203–213, 2009.
- [59]. M. Storch, F. Hinrichsen, M. Wensing, S. Will, and L. Zigan, "The effect of ethanol blending on mixture formation, combustion and soot emission studied in an optical DISI engine," *Appl. Energy*, vol. 66, pp. 77–80, 2015.
- [60]. A. K. Agarwal, A. Dhar, D. K. Srivastava, R. K. Maurya, and A. P. Singh, "Effect of fuel injection pressure on diesel particulate size and number distribution in a CRDI single cylinder research engine," *Fuel*, vol. 107, pp. 84–89, 2013.
- [61]. H. K. Suh, "Investigations of multiple injection strategies for the improvement of combustion and exhaust emissions characteristics in a low compression ratio (CR) engine," *Appl. Energy*, vol. 88, no. 12, pp. 5013–5019, 2011.
- [62]. Q. Wang, C. Yao, Z. Dou, B. Wang, and T. Wu, "Effect of intake pre-heating and injection timing on combustion and emission characteristics of a methanol fumigated diesel engine at part load," *FUEL*, vol. 159, no. July, pp. 796–802, 2015.
- [63]. . K. Wamankar and S. Murugan, "Effect of injection timing on a DI diesel engine fuelled with a synthetic fuel blend," *J. Energy Inst.*, vol. 88, no. 4, pp. 406–413, 2015.
- [64]. C. Wang, H. Xu, J. M. Herreros, J. Wang, and R. Cracknell, "Impact of fuel and injection system on particle emissions from a GDI engine," *Appl. Energy*, vol. 132, pp. 178–191, 2014.
- [65]. Y. Zhang and H. Zhao, "Investigation of combustion, performance and emission characteristics of 2-stroke and 4-stroke spark ignition and CAI / HCCI operations in a DI gasoline," *Appl. Energy*, vol. 130, pp. 244–255, 2014.
- [66]. F. Escudero, A. Fuentes, R. Demarco, J. L. Consalvi, F. Liu, J. C. Elicer-Cortés, and C. Fernandez-Pello, "Effects of oxygen index on soot production and temperature in an ethylene inverse diffusion flame," *Exp. Therm. Fluid Sci.*, 2015.