

# Modification of Manufacturing Process of Kingpin for Steering Assembly of Heavy Motor Vehicles and its Analysis

<sup>1</sup>Vinay Dilliwar, <sup>2</sup>Sankalp Verma

<sup>1</sup>M.Tech Scholar, <sup>2</sup>Sr. Assistant Professor

<sup>1</sup>Production Engineering,

<sup>1</sup>SSGI Bhilai, Chhattisgarh, India.

**Abstract:** Conventional design of kingpin comes with a cross hole in the center of pin. But when the vehicle got loaded and travelled across hilly areas it was found that vehicle developed field failure from the center of kingpin. This was due to low core hardness required in the cross-hole area. In the proposed design this cross hole is eliminated which was used only for greasing. By eliminating this cross-hole manufacturing cost also got reduced and improved lead of manufacturing also. New kingpin without cross-hole is manufactured using standard manufacturing techniques which includes process flow diagrams and PFMEA. Nondestructive testing of new design of kingpin is also conducted using MPI testing

**Keywords:** Kingpin, MPI testing, PFD, PFMEA.

## I. INTRODUCTION

The kingpin, is the main pivot in the steering mechanism of a car or other vehicle. The suspension design is crucial in the development of vehicle behaviour to optimize vehicle performance, handling and comfort. There are a multitude of possible adjustments depending on the vehicle. These settings play a important role in passengers safety in all phases of driving. The design of the steering system plays a vital role in stability and control of an automobile.

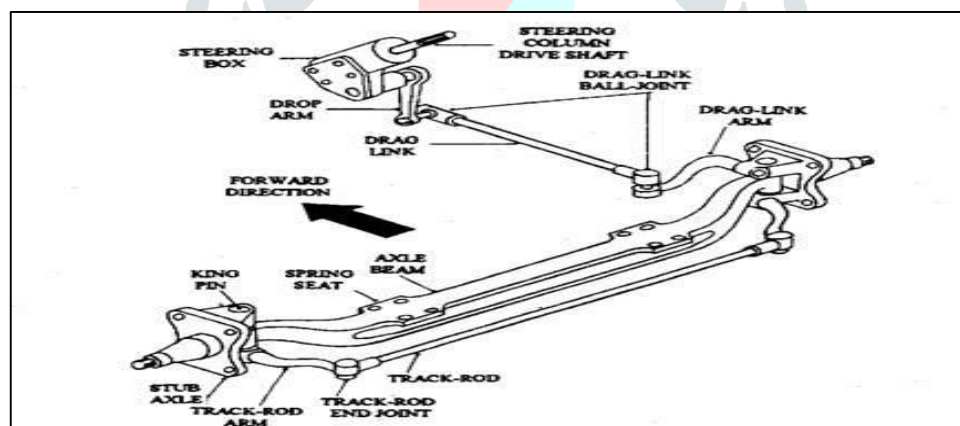


Figure 1: Kingpin location on front axle

## II. LITERATURE REVIEW

Min Jhang, Lijun Li (2015) [1] analyzed stress and fatigue life of front axle beam by finite element analysis and experimental method. Also, investigate the effect of crack parameters like length and depth on fatigue life.

Topac (2008) [2] evaluated the fatigue failure prediction and fatigue life of a rear axle housing prototype by using Finite element analysis of heavy-duty truck. The expected load cycles required to fail during the vertical fatigue tests of a rear axle housing prototype is studied and mechanical properties were determined of housing material

A.K. Acharya et al. [3] described the failure analysis of the rear axle at the root of the spline of a tractor with a loaded trolley used for haulage. The front wheel lifting and the failure of the rear axle at the root of the spline though mainly due to the transfer of weight, not sufficient attention. By reducing the hitching height and it was observed that by reducing the hitching height to 16.00 inches (which is normally taken as 19 to 20 inches) with reduction in the weight transfer factor by nearly 20%.

Sanjay Aloni et al. [4] Studied on Evaluation of Tractor Trolley Axle by Using Finite Element Analysis to modify existing rear axle of 6.0-ton tractor trolley. Fatigue failure of the rear axle finite element model was predicted after the dynamic load was imposed on it. Spectrum analysis revealed that the failed axle shaft material is SAE 1020 steel. Fractographic features indicated that fatigue

was the main cause of failure of the axle shaft. It was observed that the fatigue cracks originated from transition areas due to sharp corners.

Osman Asi et al.[5] described the failure analysis of a rear axle shaft used in an automobile which had been involved in an accident. The failure zones were examined with the help of a scanning electron microscope equipped with EDX facility. Spectrum analysis and micro-hardness measurement show that the failed axle shaft material was AISI 4140 steel as hardened and tempered condition. Fractographic features indicated that fatigue was the main cause of failure of the axle shaft. It was observed that the fatigue cracks originated from welded areas. Due to the improper welding. So improper welding of hardened materials involves low ductility in the HAZ, stress concentration points, and inclusions in the structure that served as responsible for the fatigue cracks.

### III. PROPOSED WORK

Manufacturing & Machining of kingpin using process plan as described in next following steps

1. VMC operation on fixture
2. MPI Testing
3. Induction Hardening testing (Pattern Testing)
4. Material Testing
5. Hardness Testing
6. PFD
7. PFMEA
8. Control Plan

### IV. MATERIALS AND METHODS

OPN 20 :- In this operation full length Bar of raw material cut on bandsaw machine with particular specification for reducing end piece scarp from the round bar. Below is the table for defining Process parameters & checking Method for reducing rejection & method for cutting the part on bandsaw.

OPN 30: In this operation length of the pin maintained for removing tapper from the face, So this operation is said as facing operation. Bellow are the process specifications for maintaining the dimension in part.

Table 1: Operation no. 30 details

OPN No.-30	TOOL	SPEED (rpm)	FEED (mm/min)	CHECK & CHANGE QTY..	NECESSARY ACTION	PART ID	DIMENSION	GAUGE NAME AND NO.	CHECK FREQUENCY	NECESSARY ACTION
951 KP	TNMG16	930~980	165~175	500	ACTION SHOULD BE A PART COUNT& TOOL WEAR	951 KP	138.5±0.5	DIAL TYPE HIGHT GAUGE	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA

OPN 40: In operation 40 drilling done on RDM machine for maintaining below specifications.

Table 2: Operation no. 40 details

OPN No.-40	TOOL	SPEED (rpm)	FEED (mm/min)	CHECK & CHANGE QTY..	NECESSARY ACTION	PART ID	DIMENSION	GAUGE NAME AND NO.	CHECK FREQUENCY	NECESSARY ACTION
951 KP	8 MM CHF TOOL	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	Ø 8.0 ±0.2	Vernier	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA
951 KP	8 MM CHF TOOL	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	20+2	Vernier	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA

OPPN 50: proceed on lathe machine for turning the diameter of king pin. Below are the specifications for maintaining the process parameters on machine.

Table 2: Operation no. 50 details

OPN No.-50	TOOL	SPEED (rpm)	FEED (mm/min)	CHECK & CHANGE QTY..	NECESSARY ACTION	PART ID	DIMENSION	GAUGE NAME AND NO.	CHECK FREQUENCY	NECESSARY ACTION
951 KP	TNMG16	930~980	165~175	500	ACTION SHOULD BE A PART COUNT & TOOL WEAR	951 KP	28.25 ± 0.05	Micrometer	1 in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA

OPPN 60: This operation held on Lathe machine for maintaining chamfer of the pin. Below are the process parameter specifications for manufacturing the part.

Table 2: Operation no. 60 details

OPN No.-60	TOOL	SPEED (rpm)	FEED (mm/min)	CHECK & CHANGE QTY..	NECESSARY ACTION	PART ID	DIMENSION	GAUGE NAME AND NO.	CHECK FREQUENCY	NECESSARY ACTION
951 KP	TNMG16	930~980	165~175	600	ACTION SHOULD BE A PART COUNT & TOOL WEAR	951 KP	2 ± 0.1	Part to be confirm with QC Inspection and check for Operation complete.	non recorded 100% Visual Inspection (Comparison with master)	RESET/KEEP IN NCP AREA

OPPN 70: In this operation slotting operation have been done on slotting machine. Below are the process parameters maintain for this operation

Table 3: Operation no. 70 details

OPN No.-70	TOOL	SPEED (rpm)	FEED (mm/min)	CHECK & CHANGE QTY..	NECESSARY ACTION	PART ID	DIMENSION	GAUGE NAME AND NO.	CHECK FREQUENCY	NECESSARY ACTION
951 KP	SPMG 11	190~210	145~155	600	Action should be a part count & tool wear	951 KP	DIM. 25 ± 0.5	Dial type variable Slot Depth Gauge /Radius gauge/vernier	1 in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA

OPPN 80: This Operation done on RDM Machine for maintaining drill depth & diameter. Below are the process Parameter Specifications.

Table 4: Operation no. 80 details

OPN No.-80	TOOL	SPEED (rpm)	FEED (mm/min)	CHECK & CHANGE QTY..	NECESSARY ACTION	PART ID	DIMENSION	GAUGE NAME AND NO.	CHECK FREQUENCY	NECESSARY ACTION
951 KP	11 MM CHF TOOL	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	Counter Drill 11 ± 0.2	VISUALY	1 in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA
951 KP	11 MM CHF TOOL	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	6 ± 0.2	VISUALY	1 in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA

OPPN 90: This operation is held for maintaining chamfer angle on the Pin. Below are the process parameters for maintaining the specifications.

Table 5: Operation no. 90 details

OPN No.:- 90	TOOL	SPEED (rpm)	FEED (mm/min)	CHECK & CHANGE QTY..	NECESSARY ACTION	PART ID	DIMENSION	GAUGE NAME AND NO.	CHECK FREQUENCY	NECESSARY ACTION
951 KP	11 MM CHF TOOL	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	60 @±0.5°	VISUALY	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA
951 KP	11 MM CHF TOOL	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	Dim. 2 ±0.5	VISUALY	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA

OPPN 100: In this Operation drilling & Tapping done on parts on RDM Machine for maintaining the dimensions as per the drawing, for achieving the dim. Below are the specifications of the process parameters

Table 6: Operation no. 100 details

OPN No.- 100	TOOL	SPEED (rpm)	FEED (mm/min)	CHECK & CHANGE QTY..	NECESSARY ACTION	PART ID	DIMENSION	GAUGE NAME AND NO.	CHECK FREQUENCY	NECESSARY ACTION
951 KP	6 mm Drill	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	6 ± 0.2	VISUALY	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA
951 KP	6 mm Drill	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	65 ± 2	VISUALY	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA
951 KP	M10 X 1.25 TAP	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	M10 X 1.25 mm	TPG	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA
951 KP	M10 X 1.25 TAP	150	MANUALY	1200	Action should be a part count & tool wear	951 KP	Depth 15 ±2	VISUALY	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA

OPPN 110: Hardening & Quenching done in this operation for maintain the hardness & Case depth of the King Pin as per the Drawing Specifications. Below are the Process Parameters for maintaining the hardness. MPI Checking Also done during the operation for detecting cracks in the parts.

Table 7: Operation no. 110 details

PART NO.	CURRENT AMP.	FEED MM/MIN.	QRS PROCESS (IN Psi)	FLOW (ltr/min.)	% of VOLTAGE	% of Frequency	% of POWER	% of Current	REMARKS
951 KP	78 ± 3	225 ± 25	8+2	35 ± 5	55-65	55-65	85-95	70-80	Polymer (AQUEAQUENCH-365) % SPECIFICATION :- 2-3%,MAKE-HOUGHTOUN,PH VALUE 7-10,QUENCH TEMP. 25-40 °C, TRANS NO. 15,CAPACITOR

OPPN 120: Grinding operation done on King pin for maintaining outer Diameter of the King Pin. Below are the specifications for King Pin for maintaining the process parameters.

Table 8: Operation no. 120 details

OPN No.-120	TOOL	SPEED (rpm)	FEED (mm/min)	CHECK & DRESSING QTY	NECESSARY ACTION	PART ID	DIMENSION	GAUGE NAME AND NO.	CHECK FREQUENCY	NECESSARY ACTION
951 KP	GRINDING WHEEL	250	MANUALY	100	ACTION SHOULD BE A PART COUNT& TOOL WEAR	951 KP	Ø 28-0.025/-0.064	Micrometer	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA
951 KP	GRINDING WHEEL	250	MANUALY	100	ACTION SHOULD BE A PART COUNT& TOOL WEAR	951 KP	Perpendicularity 0.015	VARIABLE DIAL HIGHT GAUGE	1in 10 check by op. in self inspection report	RESET/KEEP IN NCP AREA

OPPN 130: After completing all the operations part moved to Final Inspection area for 100% Checking of the Parts as per the inspection plan, For Knowing Dimension Results on the part. IF parts found not Ok, the the parts get Rejected & putted in NCP area.100% parts checked for MPI for Crack Detection.

OPPN 140: In this operation Pre Dispatch Inspection process held for Inspecting parts Visually.

OPPN 150: Storage will done of OK parts as per the standard procedure after packing of the material. Anti-rust oiling should be done on parts before packing in poly bag for eliminating rusting issue in parts as per customer specific requirement.

Magnetic particle inspection is nondestructive type of testing for detecting cracks on part by use of circular coil 1250 on 1400 ampere under 3.15kat and oil concentration of 0.3ml . Checking cracks by generating magnetic field on fork , applying oil flow and then visually detecting it in presence of uv rays.


M.P.I. Check Sheet		Format No.- MAPL/F/QC/110 Rev No. 00 Issue Date:- 10.03.2017	
Process Parameter details:-	1..Machine No. 01	3. Demagnetize :- Working	4. Defective Sample:-Checked
	2. Oil flow:- Yes	4. Bulb Intensity:- ok	2. Pie Testing:-Checked
	9.Oil level:-Yes	10.Calibration Status:- Yes	11.No. of Strokes :- 1
	13. Coil knob setting:- 2+2High	14. L. Knob Setting:- 3	15.Copper bush availability:- N.A
Part details	Part Length:- 180.5 mm		7. Circular coil:-Working
	Part Name: King Pin		8. L Coil :- Working
	Part Max. Dia :- 27.98mm		12.Type of Magnatized:- Combined
	Induction Batch No.- 180301		OK
Setup	Required Current:-	Circular Coil:- 1250 ± 100	L. Coil :- 3.00 Kat Min.
	Actual :-	1400 AMP	3.15 KAT
	Oil Concentrate :- 0.2~0.4 ml/ltr		0.3 ml
	SI No.	Time	Quantity
			Checked OK NOT OK
	1	8:00 PM	30 30 0
	2	9:00 PM	30 30 0
	Demagnetize		
	Loading pattern		
	Straight Fit to Coil		
Location of Crack Pattern			
			
Total			
60 60 0			
Remarks:-			
Checked By:-Mr. Radheshayam			
Approved By:-Mr Abhishek Sharma			

Figure 2: MPI testing report of Kingpin

METALMAN AUTO PVT. LTD.					Form No:		MAPL/F/PROD/13			
INSPECTION REPORT					Date:		16.12.18			
					Lot Qty:		60			
					Heat Code/Lot		S			
Part No: 951KP										
Part Name: King Pin							Critical * Major			
Visual & Dim Inspection										
Sl.No.	Parameter	Spc	Tol.	Checking Aids	Observations					Result / Remarks
					1	2	3	4	5	
1	Length	180	±0.5	Vernier	180.2	180.1	180.2	180.2	180.1	ok
2	O.D. ♂	28	-0.020 - 0.053	Micrometer	27.954	27.967	27.955	27.972	27.958	ok
3	Chamfer	2X20°		Visual	ok	ok	ok	ok	ok	ok
4	Roughness	0.8		Surface Tester	0.7	0.6	0.8	0.7	0.8	ok
5	Straightness ♂	0.015		Ht. Gauge	0.010	0.012	0.014	0.011	0.015	ok
6	Drill Depth	20	+2.0	Vernier	20.1	20.5	20.9	21	20.5	ok
7	Thread Size	M10X1.25		T.P.G.	ok	ok	ok	ok	ok	ok
8	Slot-1 Width	12	-0.5	Vernier	11.9	11.87	11.95	11.82	11.85	ok
9	Slot-1 O.D. ♂	25	±0.1	Micrometer	25.05	25.03	25.02	25.06	25.02	ok
10	Slot Distance •	112.5	±0.3	Trimos	112.7	112.5	112.2	112.4	112.5	ok
11	Thread Size	M6X1.0		T.P.G.	ok	ok	ok	ok	ok	ok
12	Visually	Burr, Dent, Rust, Finish, Operation Missing			100% Checked - TPG/Ring Gauge/Templet					
As per Sampling plan										
OK Qty :- 60				Rework Qty:- 0			Reject Qty:- 0			
Remarks (if any) : 100% checked by vaibhav										
Checked By:- Pawan Gupta					Approved By:- Abhishek Sharma					

Figure 3: Inspection report of Kingpin

 <b>METALMAN AUTO PVT. LTD.</b> <b>Material Test Report</b>		Form No.	MAPL/F/PROD/51
		Issue:	01
		Sheet No.	1/1

Report No.	180301	Date	15/04/2018
Part Name.	King Pin	Raw Material	
Part No./ Rev. No.	951KP	Raw Material Used	CK45
Material TC	Received Ok	Heat No.	08
Heat Treatment Process	Induction Hard. & Temp. (HT30T)	Quantity	60 Nos.
Induction Hardening	MAPL180301	Chemical Composition	
Batch, done & date	20.12.18	Report No. & Date	

## Induction Heat Treatment Process Parameters (as per Std.)

Machine no.	2	KW	100 KW	OK
Location	X	Location	X	
Power (kW)%	18 %	Rotation	no	
Start Heating Time	After 2 secs	Frequency KHZ	30 khz	
Heat Dwell Time	1.65 Sec	Polymer% (Without factor)	2%	
Scan Speed (Feed)	150 mm/min	Total Cycle Time	14 Sec	
Total Heating Time	2 sec	Quenching Bath Temp.	27 °C	
Total Quenching Time	8 secs	Tempering Temp.	160°C @ 90 min.	



Quality requirements for induction hardening for 'X' (as per std.)			
Test	Specification	Observation	Remark
Hardness	19 – 36 HRC	31 - 35 HRC	OK
Case Depth @ X Loc.	1± 0.2 @ 550HV	Sec.1	A = 1.1 mm
			B = 1.08 mm
		Sec.2	A = 1.01 mm
			B = 1.05 mm
MPI	No Crack	No Crack Found	OK

**Metallographic Observation:**

PARAMETERS	SPECIFICATIONS	OBSERVATIONS	REMARKS
Case Microstructure	Fine tempered martensite (RA < 5%, no Carbides)	Tempered martensite with RA ~5% , no Carbides	OK
Core Microstructure	Low carbon marten site / Bainite	Low carbon marten site no ferrite	OK
Inclusion Rating	≤ 2 ABCD	1.5A, 1.0 B, 1.0D	OK
Magnafluxing / acid etching /Visual	Shall be free from cracks, under cut, sharp edges etc	No Such defects observed	OK

Remark: No Crack Observed during inspection & As per Specifications Part Sample found Ok.

Checked By: Ashish

Approved By: Abhishek Sharma

Figure 4: Material Testing report of Kingpin

Developing and verifying hybrid drives a new level of technology from driveline test rigs. The Driveline can test hybrid systems for the task using Secondary Control Technology. Secondary Control allows hydraulic systems to quickly switch from absorption to driving thus the rig can replicate realistic drive cycles in order to optimize hybrid drives. Manufacturers of hybrid drive systems will be able to work on their regenerative control strategies by using driveline rig in drive cycle replication mode. To allow energy management controller development, the drive cycle can be created manually or by using data previously recorded on an instrumented Commercial Vehicle. Thus, the efficiency of the hybrid drive system through the complete cycle is measured. This allows our customers to try different energy management strategies in the controllers to fully optimize their performance

## V. CONCLUSION

The Induction hardening analysis is conducted on kingpin by using material destructive testing and results obtained shows that King Pin without cross Hole performs better as compared with King Pin with cross hole. Removal of Cross Hole has also helped in manufacturing process reduction. Along with that the rejection rates which were higher in Cross Hole which is drastically reduced. Thus, the removal of slots has aided in reducing manufacturing process and rejection and high compactness is achieved which lead to better interference fit in assembly line and lower rejection rates during manufacturing. The experimental analysis is also conducted using driveline rig and results obtained are in close agreement with simulation results.

## REFERENCES

- [1]. Min Zhang, Xiangfei Ji, Lijun Li, A research on fatigue life of front axle beam for heavyduty truck, Advances in Engineering Software 91 (2016) 63–68
- [2]. M.M. Topac , H. Gunal , N.S. Kuralay, Fatigue failure prediction of a rear axle housing prototype by using finite element analysis , Engineering Failure Analysis 16 (2009) 1474–1482 [8]. Leon, Reducing the Weight of a Frontal Truck Axle Beam Using Experimental Test Procedures to Fine Tune FEA, MSC Automotive Conference., 2010.
- [3]. A.K.Acharya, I. Panigrahi, P. C. Mishra, “Failure analysis of rear axle of a tractor with loaded trolley”, international journal of innovative research & development Vol 2 Issue 10ISSN;2278-0211 oct-2013.
- [4]. Sanjay Aloni and Sandip Khedkar “Comparative evaluation of tractor trolley axle by using Finite Element analysis approach”, International Journal of Engineering Science and Technology.vol-4,ISSN:0975-5462, April-2012.
- [5]. Osman Asi, “Fatigue failure of a rear axle shaft of an automobile”, Engineering Failure Analysis 13 (2006) .pp 1293– 1302.