

RESPONSE STUDY OF NATURAL DRAFT HYPERBOLIC COOLING TOWERS UNDER WIND LOADS: A REVIEW

¹Kinchit Soni,²Dr. Suhasini Kulkarni

¹PG Student,²Associate Professor,

¹Civil Engineering Department,

¹Parul University, Vadodara, India.

Abstract: Basically, cooling tower is a device which extract waste heat from industry or plant building to the atmosphere through cooling of water stream at a lower temperature. As these are very huge thin shell structures, they basically subjected to its self-weight and the dynamic loads as an earthquake load and wind load. Recent devastating occurred earthquakes have vulnerable effects on cooling towers and played vital role of them in safety and performance of power plants during and after a strong ground motion. The cooling tower has been analyzed for the wind load as well as the seismic load by using the finite element analysis of ANSYS version by assuming its bottom end fixed and top end free to displace. As a part of analysis, cooling tower of height 143.50 m is taken of having different column supporting systems i.e. H-frame, V-frame, I-frame, A-frame. The effect of wind load on the cooling tower is considered by defining design wind pressure coefficients given in IS: 11504-1985 along with the pressure distribution at various heights as per given in IS: 875-Part III-1987. Seismic load is carried out by applying 0.5g in accordance with the IS: 1893-2016. For the purpose of comparison, maximum principle stresses, shear stresses and deformation of tower are derived from the analysis.

Index Terms - Hyperbolic cooling tower, ANSYS WORKBENCH, I-frame, H-frame Support, Wind load, Throat location, Stiffeners.

I. INTRODUCTION

Cooling tower is a heat rejection device, which extracts waste heat to the atmosphere through the cooling of a water stream to a lower temperature. Common applications for cooling towers are providing cooled water for air-conditioning, manufacturing and electrical power generation. R/C cooling towers are subjected to its self weight and the dynamic load such as an earthquake motion and a wind effects. Especially, dynamic analyses of these structures are important factor to design R/C cooling tower structures. Especially, dynamic analyses of these structures are important factor to design R/C cooling tower structures. The structures have huge surfaces of concrete with increasing its constructional height and also, R/C shell structure is usually placed on the supporting columns to take a cold air into it. R/C cooling tower represents the combinations of R/C shell and R/C column structures. The progressive nature of the corrosion-induced deterioration, understanding the root cause, the consequences and associated costs was essential. As such, a condition evaluation was conducted. The total weight of the tower and the static pressure on each column also was determined. Utilizing the collected data, the tower was recreated using a three-dimensional structural engineering computer program. The software included model generation, static, dynamic and linear analyses. Dynamic behavior of R/C cooling tower shell under an earthquake loading is analysed by use of FEM. The most common sight, especially in power plants and nuclear plants, is hyperboloid-shaped cooling towers. The hyperboloid shape impacts the strength of the entire structure. Since cooling towers are supposed to cool the working fluid down to a low temperature, they release vapours into the atmosphere through the opening at the top of the tower. Therefore, these towers have to be sufficiently tall (they can be as tall as 200 meters), or else the released vapour may cause fogging or recirculation. To support such a high structure, it is extremely important that the base is considerably consolidated and spread over a large area so that it can support the tall, heavy structure above it. This is why cooling towers have a large, circular base.

Why hyperbolic shape preferred?

Hyperbolic shape helps in facilitating aerodynamic lift and ensures faster and more efficient diffusion into the atmosphere. There are also some other reasons behind the usage of this shape. For example, a wide base not only provides strength to the whole structure, but also offers ample space for the installation of machinery. From a logistical standpoint, this shape is easier to build, as it employs a lattice of straight beams to erect the tower. Also, this type of structure is more resistant to external natural forces than straight buildings.

All cooling towers are designed to remove waste heat from water and transfer it to the atmosphere, but there are a lot of ways to accomplish this task. Cooling towers can be categorized in a number of different ways, because there are so many differences between cooling towers. For our purposes, we will cover three kinds of cooling towers based on how air and water flow (counter flow, cross flow, and hyperbolic) and two types based on how the air is moved (mechanical and natural draft).

Geometry of Cooling Towers:

The geometry of the Hyperboloid revolution,

$$\frac{R_0^2}{a_0^2} - \frac{y^2}{b^2} = 1$$

In which is the horizontal radius at any vertical coordinate, Y with the origin of coordinates being defined by the center of the tower throat, is the radius of the throat, and b is some characteristic dimension of the hyperboloid.

Load calculation:

Other than self-weight, the external applied loads that affect the cooling tower are dead loads, wind loads, effect of adjacent structures, imposed loads, foundation settlement loads, constructional loads, and thermal loads. The predominant forces acting on the cooling tower will result from wind or seismic loading. The reinforcement design of cooling tower is often controlled by the net difference between the tension due to wind load and compression due to dead load.

Wind force forms the major external applied loading in the design of cooling towers, and it also provides the most common means of determining the degree of lateral strength required by the towers. Wind load is calculated as pressure acting on each plate. Both vertical and circumferential variation if wind pressure is considered. The vertical variation if wind pressure is given by IS 875 – part 3 – 1987. And circumferential variation of wind pressure is given by IS 11504 – 1985.

Vertical Wind pressure distribution:

IS 875 (Part 3) – 1987 determines wind pressures based on peak wind speed of 3 second gust with a return period of 50 years. The zones of basic wind speed at 10 m above ground at speeds of 33, 39, 44, 50 and 55 m/s are shown in the code on a wind map of the country. The design wind speed is calculated by considering the factors k1, k2, k3 related to probable life of structure, terrain, local topography and size of structure separately, and their combined effect is determined by multiplying the factors, the design wind pressure at any height above mean ground level shall be obtained by the following relationship between wind pressure and wind velocity:

$$P_z = 0.6 V_z^2$$

Where

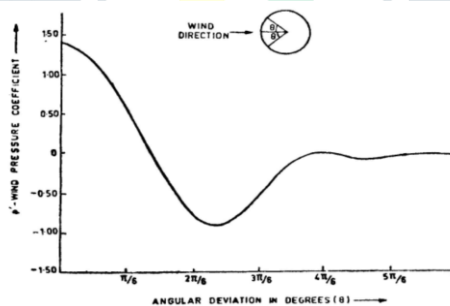
P_z = design wind velocity in N/m² at height z, and
 v_z = design wind velocity in m/s at height z.

Design Wind Speed (V_z) is The basic wind speed (V_b) for any site shall be modified to include the effects of risk level, terrain roughness, height and size of structure and local topography to get design wind velocity at any height (V_z) for the chosen structure.

$$V_z = V_b \cdot k_1 \cdot k_2 \cdot k_3$$

V_z = design wind speed at any height z in m/s;
 k1 = probability factor (risk coefficient),
 k2 = terrain, height and structure size factor and
 k3 = topography factor.

Circumferential wind pressure distribution:



IS 11504 – 1987 gives the coefficient for circumferential variation of wind pressure in hyperbolic cooling towers. As per the code (clause 5.1.3 and 6.2 - A- 2), the wind pressure distribution on the outside of the shell is assumed to be symmetrical about the center line in the direction of wind.

For practical design these values may be increased by 10 percent to take into account geometrical imperfections. The wind pressure coefficient distribution around the shell is defined by the following graph Circumferential Wind Pressure Coefficient Distribution. The distribution shall be used at all heights of the tower and includes an allowance for internal suction.

$$p' = \sum_{n=0}^7 F_n \cdot \cos n\theta$$

P' = design wind pressure coefficient,
 F_n = Fourier coefficient of nth term, and
 θ = angular position measured from the incident wind direction in degrees.

Values of F_n for various values of n are tabulated below:

N	F_n
0	-0.00071
1	+0.24611
2	+0.62296
3	+0.48833
4	+0.10756
5	-0.09579
6	-0.01142
7	+0.04551

With various values of F_n from the table, circumferential wind distribution coefficient for each 2.5° angle difference is calculated. Variation of the coefficient (p') in the structure's cross section. The coefficient is maximum at incident 0° and it slowly reduces below 0 and attains negative maximum (Suction) around 75° .

Circumferential variation of wind pressure:

The actual design wind pressure on the shell is obtained by multiplying the basic wind pressure as given in IS: 875 by the coefficient p' . Hence individual values of pressure acting on all 2880 plates are calculated.

Dynamic effects of wind:

As per IS 875 (Part 3) – 1987, Clause 7.1 Flexible slender structures and structural elements shall be investigated to ascertain the importance of wind induced oscillations or excitations along and across the direction of wind. In general, the following guidelines may be used for examining the problems of wind induced oscillations:

- Buildings and closed structures with a height to minimum lateral dimension ratio of more than about 5.0, or
- Buildings and structures whose natural frequency in the first mode is less than 1.0 Hz. (Natural frequency is $(1/T)$, whereas the fundamental time period (T) may either be established by experimental observations on similar buildings or calculated by any rational method of analysis) Any building or structure which satisfies either of the above two criteria shall be examined for dynamic effects of wind. If preliminary studies indicate that wind-induced oscillations are likely to be significant, investigations should be pursued with the aid of analytical methods or, if necessary, by means of wind tunnel tests on models.

Effect of adjacent structures:

For taller and larger cooling towers the effect of adjacent structures in wind load plays a vital role, and hence it is important to derive the wind pressure distribution on the structure from wind tunnel experiments. Also for towers built at closer spacing, it is suggested to determine wind pressure distribution by model tests in a wind tunnel offering appropriate aerodynamic similitude. Such models shall include all adjacent topographical features, buildings and other structures which are likely to influence the wind load pattern on the tower significantly. This effect is not considered in this project.

CONCLUSION

- The base diameter, air intake opening height, tower height and throat diameter are determined by thermal considerations. Hence optimizing the location of throat is highly necessary in structural and economic considerations.
- Circumferential and meridional variation of both SX and SY shows that location of throat influences the stresses induced in cooling tower shell significantly.
- Variation of SX along height shows that the effect of throat variation is much in the bottom of the cooling tower and it gradually reduces to zero as we go to the top of cooling tower.
- Economical design with respect to SX would be to have a relatively lower throat and at the same time whose meridional reinforcement requirement at bottom is close to minimum reinforcement requirement. This gives additional benefit due to lower SX above shell mid-height.
- Hoop stresses are highly affected by changes in throat location mainly at throat level. Hoop stress variation is such that, higher throat location is not economical in incident face of cooling tower. Whereas very low throat location is not economical on the suction face.
- The effect of throat variation is significant at throat than it is at bottom and top of cooling tower. At top level both incident face and suction face are subjected to higher hoop stresses. This implies the significance of providing an upper ring beam.
- The range provided for throat location in the tower design considerations given by IS 11504 can be used for towers of height less than 100m. For taller towers, optimization of throat location is required as it plays a vital part in the structural safety and economy.

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