

# Study of Flow Over Sedan Car Body by Changing Different Parameters Using Open Foam

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**Abstract**—One of the major factor that determine fuel efficiency of a ground vehicle is its aerodynamic drag. Here interest was to study the aerodynamic performance of car geometry for both hatchback and sedan type vehicles and by changing their different parameters Drag force and Lift force were calculated by using CFD Software OpenFOAM. This study involves variation of geometrical features, such as hood angle, wind screen angle, rear angle, and corner radius. Car geometries were created in OpenFOAM itself by using blockMesh. Meshing was done by using snappyHexMesh. Total 14 sedan geometries were used. Comparison was made to find the geometry with least drag

**Keywords:** OpenFOAM, Drag force, Lift force, blockMesh, snappyHexMesh

## I. INTRODUCTION

"Aerodynamics" is a branch of fluid dynamics concerned with studying the motion of air, particularly when it interacts with a moving object. Aerodynamics is also a subfield gas dynamics, with much theory shared with fluid dynamics. Aerodynamics is often used synonymously with gas dynamics, with the difference being that gas dynamics applies to all gases. Understanding the motion of air (often called a flow field) around an object enables the calculation of forces and moments acting on the object. Typical properties calculated for a flow field include velocity, pressure, density and temperature as a function of position and time. By defining a control volume around the flow field, equations for the conservation of mass, momentum, and energy can be defined and used to solve for the properties. The use of aerodynamics through mathematical analysis, empirical approximation and wind tunnel experimentation form the scientific basis.

To save the energy and to protect the Global environment, fuel consumption reduction is a primary concern of the modern car manufacturers. Decreased resistance to forward motion allows higher speed for the same power output, or lower power output for the same speed. The shape is an important factor for drag reduction. To design an efficient shape of the car that will offer a low resistance to the forward motion, the most important functional requirement today is the low fuel consumption. The resistance, termed as the drag force (or the drag coefficient in non dimensional terms), is a strong function of the shape of the car. This suggests it is important how the fluid particles move about the car and how fast they move along their path.

This paper mainly concentrates on the external surface of the car geometries. Interest was to create the geometries by changing various parameter such as wind screen angle, front hood angle, rear hood angle, front corner radius etc. The evaluation of coefficient of drag, coefficient of lift, drag force, lift force can done by using OpenFOAM. software.

## II. METHODOLOGY

The OpenFOAM (Open Field Operation and Manipulation) CFD toolbox is used to analyse the airflow around the the car geometries for both Hatchback and Sedan. OpenFOAM has extensive range of features to solve anything complex fluid flow involving chemical reactions, turbulence, and heat transfer to solid dynamics and electromagnetics.

The car geometries having different external parameters are created in OpenFOAM itself by using blockMesh. It is then converted into the stereolithography (STL) file. STL file is then linked to snappyHexMesh for generation of mesh. potentialFoam was used to generate initial flow. By giving initial boundary conditions calculations were done by using simpleFoam and finally postprocessing was done by using ParaFoam.

The velocity and pressure distribution over the geometries are visualized and discussed. Through the aerodynamic analysis a contour of pressure and velocity that impacts the car body is studied. Then accordingly coefficient of drag, coefficient of lift, drag and lift force are calculated. For the flow analysis the tyre portion is not taken into the consideration.

## III. MATHEMATICAL FORMULATION

### Drag Force ( $F_D$ )

Aerodynamic drag force is the force acting on the vehicle body resisting its forward motion. This force is an important force to be considered while designing the external body of the vehicle, since it covers about 65% of the total force acting on the complete body. The drag coefficient is dimensionless quantity that describes vehicle aerodynamic resistance and is useful tool for comparing different vehicle shapes. The Aerodynamic drag force is calculated by the following formula:

$$F_D = \frac{1}{2} \rho V^2 C_D A \quad (3.1)$$

where:

$F_D$  = Drag Force

$C_D$  = Drag Coefficient

A = Frontal Area Of The Vehicle  
 V = Wind Velocity  
 ρ = Air Density

**Lift Force (F<sub>L</sub>)**

Lift force causes the vehicle to get lifted in air as applied in the positive direction, whereas it can result in excessive wheel down force if it is applied in negative direction. Engineers try to keep this value to a required limit to avoid excess down force or lift. The formula usually used to define this force is written as:

$$F_L = \frac{1}{2} \rho V^2 C_L A \tag{3.2}$$

where:

F<sub>L</sub> = Lift Force  
 C<sub>L</sub> = Lift Coefficient  
 A = Frontal Area Of The Vehicle  
 V = Wind Velocity  
 ρ = Air Density

**For sedan geometry**

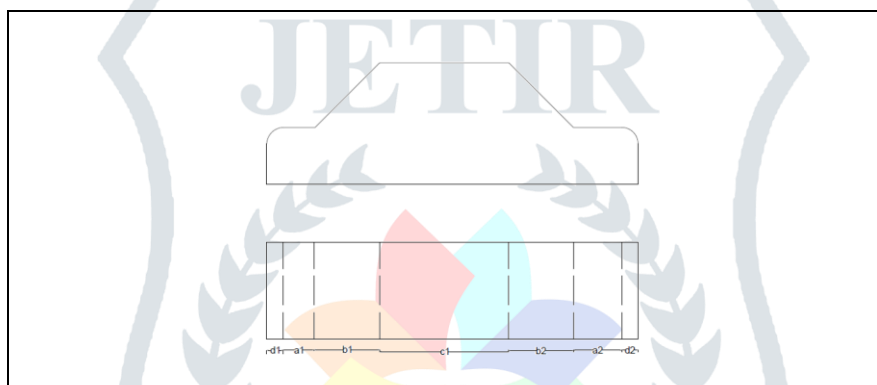


FIG 1.GEOMETRY OF HATCHBACK

Table 1 .Parameters for Hatchback geometry

Case No.	b1	b2	Radius	Hood angle	Rear angle
1	0.1	0.1	0.01	0	-
2	0.2	0.2	0.01	0	-
3	0.2	0.2	0.01	0	-
4	0.4	0.4	0.01	0	-
5	0.3	0.3	0.01	0	-
6	0.3	0.3	0.15	0	-
7	0.3	0.3	0.1	0	-
8	0.3	0.3	0.1	5	-
9	0.3	0.3	0.1	10	-
10	0.3	0.3	0.1	15	-
11	0.3	0.3	0.1	20	-
12	0.3	0.3	0.1	10	10
13	0.3	0.3	0.1	10	15
14	0.3	0.3	0.1	10	20

### Computational set up

Different cases were considered in order to achieve the given goals. However, the simulation setup is the same for all the cases and hence the procedure is same for all cases. The first step required to begin a new simulation is to input the actual mesh into the file structure of OpenFOAM. But in our project we are creating the geometry in OpenFOAM itself by using blockMesh. It is then converted into the stereolithography (STL) file.

### Domain specifications

The computational domain is designed to lead to a free flow with neglectable blockage, which essentially means a box that consist of a inlet, a outlet, two sides, a roof and ground surface. When the geometry was defined in the creation of the computational mesh, all faces of the domain were assigned names. The names of the inlet and outlet planes (at  $x = 0$  and  $x = L$ ) are front face and back face of domain as velocity inlet and pressure outlet respectively. The names of the planes at  $y = L$ ,  $z=0$ , and  $z=L$  are outer wall as wall. The names of the model are car as a wall.



Fig.2 Defining the Domain

### Mesh

Mesh is created using snappyhexmesh, OpenFOAM's native meshing tool. Utility snappyHexMesh is used to create high quality hexdominant meshes based on arbitrary geometry. It is controlled by parameters in the le snappyHexMeshDict. It can be executed in parallel. It preserves the feature edges, addition of wall layers. Details of mesh size is given in the following table.

Table 2 Details of mesh size

No. of points	No. of cells	No. of faces	No. of internal faces
1969583	1824778	5617183	5515085

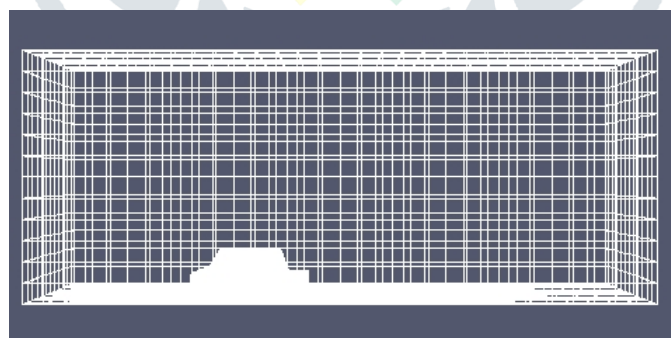


Fig.3 Side view after meshing

### Boundary conditions

The tests were taken at different operating speed range such as 60 km/hr, 70 km/hr, 80 km/hr, 90 km/hr, 100 km/hr, 110 km/hr, 120 km/hr, 130 km/hr. That means each geometry of hatchback can pass through these speed range. For example consider case 1 when it pass through 60km/hr, velocity of the inlet boundary condition is set with value 60km/hr (16.16m/s) with temperature of 300K (26.85°C). The outlet boundary condition is set to pressure outlet with gauge pressure of 0 pa. The density of the air is set as 1.125kg/m<sup>3</sup> and the viscosity of the air is 1.7894×10<sup>-5</sup> kg/(ms).

### Turbulence Modeling

All of the simulations took turbulence into account with the k- $\omega$ -SST turbulence model. This model was used for its  $\omega$  proven reliability in separation zones and its ability to blend a good freestream model to a good boundary layer model.

**Turbulence Intensity**

The turbulence intensity,  $I$ , is defined as the ratio of the root-mean-square of the velocity fluctuations,  $u'$ , to the mean free stream velocity,  $u$ .

$$I = \frac{u'}{u} \tag{3}$$

For internal flows the value of turbulence intensity can be fairly high with values ranging from 1% - 10% being appropriate at the inlet. The turbulence intensity at the core of a fully developed duct flow can be estimated as:

$$I = 0.16Re^{-1/8} \tag{4}$$

For external flows the value of turbulent intensity at the freestream can be as low as 0.05% depending on the flow characteristics. We are considering turbulence intensity as 0.02%.

**About Turbulence Length Scale** The turbulence length scale,  $l$ , is a physical quantity which represents the size of the large eddies in turbulent flows. Empirical relationship between the physical size of the obstruction (or characteristic length),  $L$ , and the size of the eddy,  $l$ , can be used to get an approximate length scale.

$$l = 0.07L \tag{5}$$

**Turbulent Kinetic Energy(K) and Specific Dissipation Rate ( $\omega$ )** Required Turbulent Kinetic Energy(K) and Specific Dissipation Rate ( $\omega$ ) can be found out from the following equations and table no.5.2 gives the (K) and ( $\omega$ ) for our selected operating speed range.

$$\text{Turbulent Kinetic Energy (K)} = \frac{3}{2}(UI)^2 \tag{6}$$

$$\text{Specific Dissipation Rate } (\omega) = \frac{K^{1/2}}{c\mu^{1/4} \times l} \tag{7}$$

Table 2 values of K and  $\omega$

Sr. no.	Speed in km/hr	Speed in m/sec	K	$\omega$
1	60	16.16	0.1665	1.061
2	70	19.44	0.2268	1.2421
3	80	22.22	0.2962	1.4197
4	90	25	0.375	1.5972
5	100	27.27	0.4629	1.7747
6	110	30.55	0.56	1.9522
7	120	33.33	0.666	2.1296
8	130	36.11	0.7824	2.3071

**RESULT AND DISCUSSION**

Comparison of sedan geometries at 100km/hr - In this comparison of selective geometries of sedan at speed of 100 km/hr and there pressure contour, velocity contour, and vector plot , are pressure variation was observed.

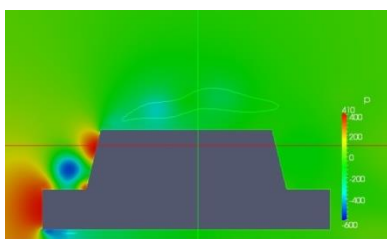


Fig.4 Case 1 Pressure contour

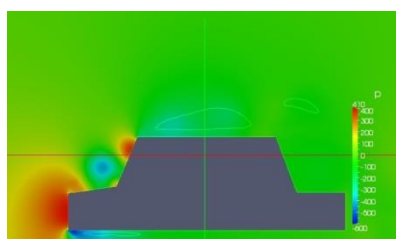


Fig.5 Case 8 Pressure contour

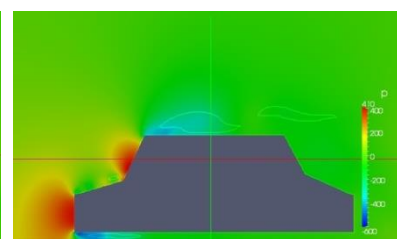


Fig.6 Case 13 Pressure contour

**Pressure contour** - It is obvious from all the pressure contours that there was a higher pressure concentration on the front of the car. Particularly, the air slows down when it approaches the front of the car and results in that more air molecules are accumulated into a smaller space. Once the air stagnates in front of the car, it seeks a lower pressure area, such as the sides and top of the car. as the air flows over the car hood, pressure is decreasing, but when reaches the front windshield, it increases briefly.

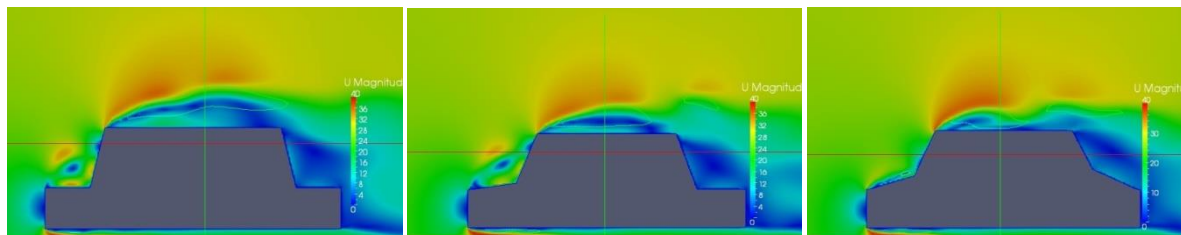


Fig.7 Case 1 Velocity contour

Fig.8 Case 8 Velocity contour

Fig.9 Case 13 Velocity contour

**Velocity contour**- It is concluded from all the velocity contours that air velocity is decreasing as it is approaching the front of the car. Then air velocity increases away from the car front.

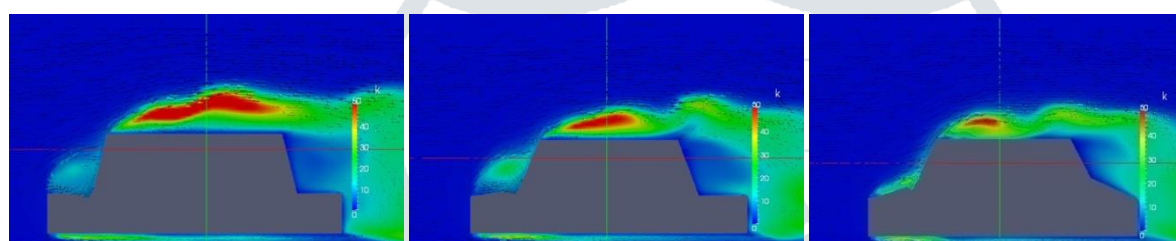


Fig.10 Case 1 Vector plot

Fig.11 Case 8 vector plot

Fig.12 Case 13 Vector plot

**Vector plot for K.E.** - From these plots it is concluded that the geometries having flat hood, large amount of turbulence is created at the front of the windscreen. On the other hand geometries having certain amount of hood angle the intensity of turbulence is minimum. The red vectors has maximum kinetic energy while blue vectors has minimum.

**Coefficient of drag and drag force for sedan geometries.**

Table 3 coefficient of drag for sedan geometry

Sr.no.	Speed in km/hr	C <sub>d</sub>				
		Case 1	Case 2	Case 3	Case 4	Case 5
1	60	0.773397	0.753260	0.704719	0.753261	0.637298
2	70	0.774616	0.754002	0.705026	0.754002	0.638238
3	80	0.774893	0.753667	0.706062	0.753667	0.63779
4	90	0.775855	0.754248	0.705861	0.754248	0.649162
5	100	0.775803	0.754321	0.705725	0.754321	0.647723
6	110	0.776412	0.754326	0.70483	0.754326	0.642182
7	120	0.776424	0.75527	0.707266	0.75527	0.643115
8	130	0.776825	0.758497	0.708452	0.758497	0.644233
Sr.no.	Speed in km/hr	C <sub>d</sub>				
		Case 6	Case 7	Case 8	Case 9	Case 10
1	60	0.668379	0.637298	0.597057	0.673109	0.662223
2	70	0.667605	0.638212	0.638239	0.672117	0.6602
3	80	0.668799	0.63779	0.596861	0.67203	0.657873
4	90	0.66888	0.649162	0.59617	0.672249	0.656926
5	100	0.668595	0.647723	0.59292	0.669132	0.65323
6	110	0.669026	0.642182	0.591991	0.671725	0.641137
7	120	0.6631	0.643115	0.589643	0.671652	0.636215
8	130	0.6632	0.644229	0.588826	0.6729	0.645107

Table 4 coefficient of drag for sedan geometry

Sr.no.	Speed in km/hr	$C_d$			
		Case 11	Case 12	Case 13	Case 14
1	60	0.602449	0.67932	0.69258	0.698741
2	70	0.602438	0.678206	0.692558	0.698268
3	80	0.602662	0.676948	0.691374	0.697306
4	90	0.603825	0.676791	0.691108	0.697255
5	100	0.604661	0.675238	0.685684	0.695947
6	110	0.603484	0.672739	0.690649	0.699227
7	120	0.604806	0.672865	0.691623	0.699804
8	130	0.604596	0.678056	0.693684	0.701509

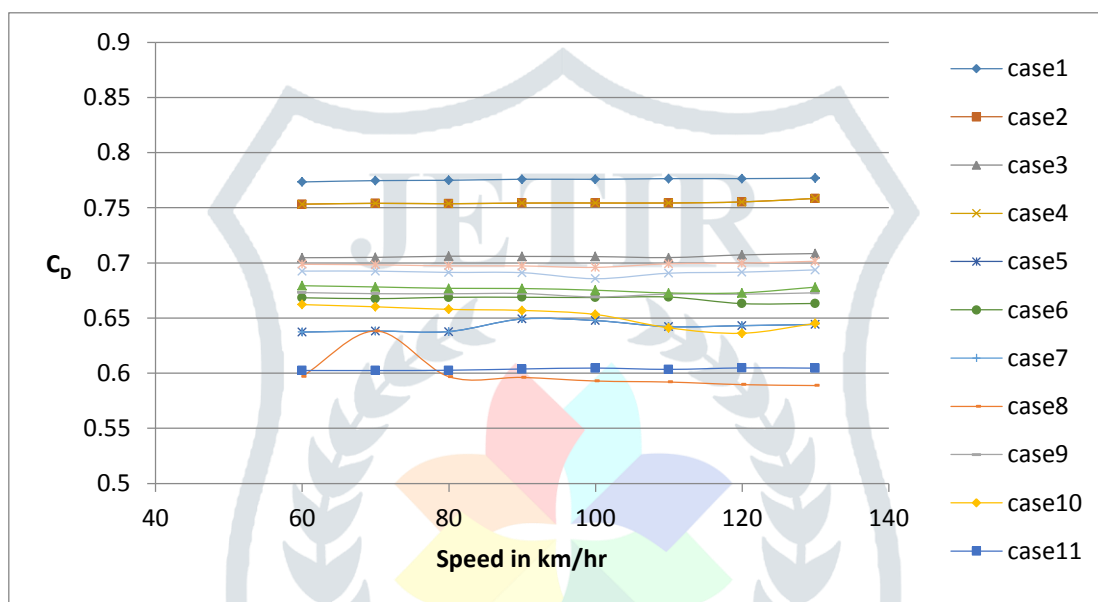


Fig 13 Comparison of all  $C_D$  for various cases V/S Speed

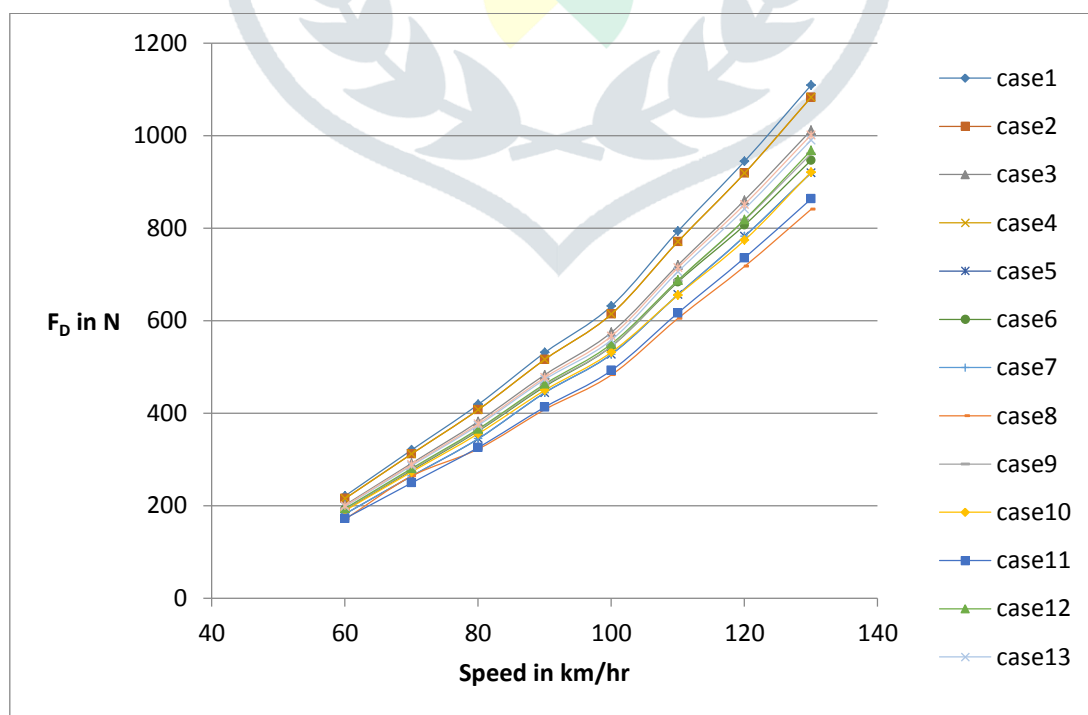


Fig 14 Comparison of all  $F_D$  for various cases V/S Speed

From the above graphs it is concluded that coefficient of drag  $C_D$  remain nearly constant for most of the cases with increase in the speed. For very few cases there will be the fluctuation of coefficient of drag with the speed. As far as drag force is concern it increases as the speed gets increased.

## CONCLUSION

The guidelines pointed out in the text are of a general nature that can be implemented in most modern road going vehicles; Smooth vehicle shape, rounded corners, high angle for the windscreen, tapered rear end, minimized body seams. Use of rear screen angle allows a reduction in aerodynamic drag of the vehicle model. Drag reducing equally depends on configuration, dimensions and arrangement of screens as well as on model's rear part configuration.

## ACKNOWLEDGMENT

The authors would like to present their sincere gratitude towards the Faculty of Mechanical Engineering in Rajarshi Shahu College of Engineering, Pune.

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